

MAGNETIC CIRCUITS

- For ~~circuits~~^{applications} with symmetry, calculating H is reasonably straight forward.
- Not so for more general case
- \Rightarrow we develop magnetic circuit theory so we can solve magnetic circuits like electrical ones

Components.

Electrical

Voltage

Resistance

Current

Ohm's Law

Magnetic

Magneto motive force (MMF)

For a coil of N turns, with current i

$$\mathcal{F} = Ni$$

Reluctance

Measures ratio between \mathcal{F} and ϕ

For a straight component,

$$\mathcal{R} = \frac{l}{\mu A}, \text{ where } l \text{ is the length}$$

Flux, ϕ

$$\mathcal{F} = \mathcal{R} \phi$$

EXAMPLE



Since the flux is always ~~to~~ along a circle, if we take the centreline, the equiv. length of the toroid is

$$l = 2\pi R$$

Its area is $A = \pi r^2$

$$\Rightarrow \text{Reluctance is } R = \frac{l}{\mu A} = \frac{2R}{\mu r^2}$$

MMF is $\mathcal{F} = Ni$

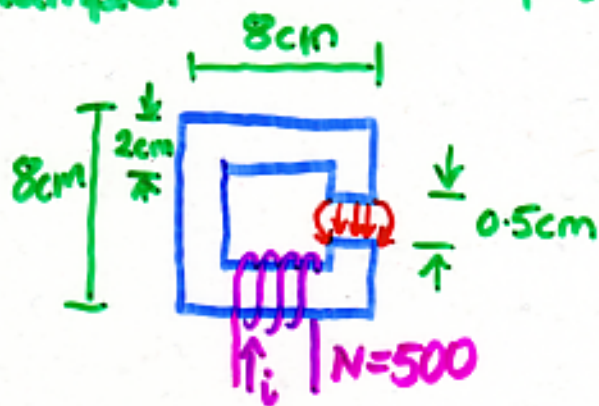
$$\Rightarrow \text{Flux is } \phi = \frac{\mathcal{F}}{R} = \frac{\mu N r^2 i}{2R}$$

Equiv. circuit



The big advantage is that we can use these concepts for non-symmetric arrangements

Example. - Iron loop with air gap and ~~square~~ $2\text{cm} \times 3\text{cm}$ cross-section



~~Find the current required to produce a flux density of 0.25 T in the air gap.~~
 Find the current required to produce a flux density of 0.25 T in the air gap.
 $\mu_{\text{core}} = 6000 \mu_0$

We would like to do this using magnetic circuit concepts.

Equiv. circuit



Thus circuit techniques will give relationship between i and ϕ .

what ϕ do we need?

$$\phi = B_{\text{gap}} A_{\text{gap}}$$

$$B_{\text{gap}} = 0.25 \text{ T}, \text{ what is } A_{\text{gap}}$$

Cross sectional area of iron loop is $2\text{cm} \times 3\text{cm}$.

However flux lines "bow" out in air gap.

- called fringing

\Rightarrow effective area is larger than core cross-section

- although we could try to compute these quantities via integration, ~~the~~ a standard approximation is to form effective area by adding length of gap to each dimension

ie, effective $A_{\text{gap}} = 2.5 \times 3.5 \text{ cm}^2$
 $= 8.75 \times 10^{-4} \text{ m}^2$.



Thus the required flux is

$$\phi = BA = 2.188 \times 10^{-4} \text{ Wb}$$

Now we can answer question by finding the required MMF.

$$F = \phi R$$

$$\Rightarrow \text{and } F = Ni$$

$$\Rightarrow i = \frac{\phi R}{N} = \frac{2.188 \times 10^{-4} R}{500}$$

All we need now is R

As you might guess, reluctances in series add.

$$\Rightarrow R = R_{\text{core}} + R_{\text{gap}}$$

$$R_{\text{gap}} = \frac{l_{\text{gap}}}{\mu_{\text{gap}} A_{\text{gap}}}$$

$$\mu_{\text{gap}} \approx \mu_{\text{vacuum}} = 4\pi \times 10^{-7}$$

$$l_{\text{gap}} = 0.5 \text{ cm}, \quad A_{\text{gap}} = \text{effective area.}$$

$$\Rightarrow R_{\text{gap}} = 4.547 \times 10^6$$

If we model the core as a sequence of straight reluctances,

$$\begin{aligned} \text{mean length} &= 4 \times 6 - 0.5 \text{ cm} \\ &= 23.5 \text{ cm} \end{aligned}$$

$$A_{\text{core}} = 2 \times 3 \text{ cm}^2 = 6 \times 10^{-4} \text{ m}^2$$

$$\mu_{\text{core}} = 6000 \mu_0 = 7.54 \times 10^{-3}$$

$$\Rightarrow R_{\text{core}} = 5.195 \times 10^4$$

Note that $R_{\text{core}} \ll R_{\text{gap}}$

$$R = R_{\text{core}} + R_{\text{gap}} = 4.6 \times 10^6$$

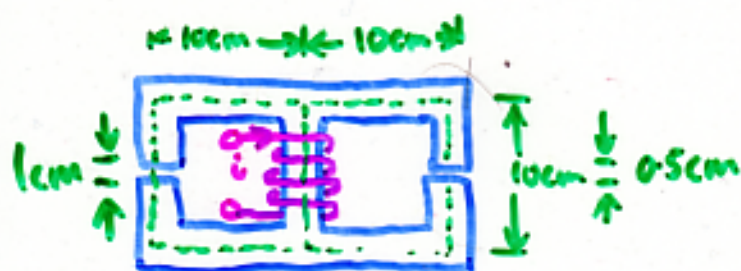
⇒ required MMF is

$$\mathcal{F} = \phi R = 1006 \text{ Aturns.}$$

$$\Rightarrow i = \frac{\mathcal{F}}{N} = 2.012 \text{ A.}$$

Note that most of the MMF is "dropped" over the air gap.

EXAMPLE



An iron core has a $2\text{cm} \times 2\text{cm}$ cross section, ~~permeability~~ means dimensions as shown, permeability $1000 \mu_0$

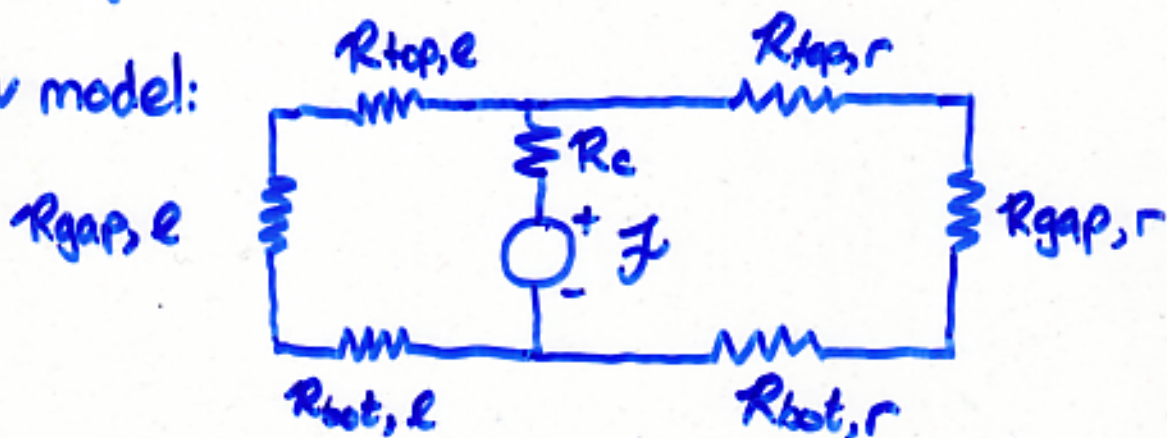
Coil has 500 turns, 2 A
Find B in each gap

Solution:

- ① Find magnetic equiv. circuit, with MMF and reluctances.
- ② Find ϕ via $\phi = \mathcal{F}/\mathcal{R}$
- ③ Find B via $B = \phi/A$.

Circuit structure

- Centre strut contains MMF and a common reluctance.
- Left + right loops have different reluctances
- Equiv model:



$$\text{MMF: } \mathcal{F} = Ni = 1000 \text{ Aturns.}$$

$$R_c = \frac{l_c}{\mu A_{\text{core}}} = \frac{10 \times 10^{-2}}{1000 \mu_0 \times 4 \times 10^{-4}} = 1.989 \times 10^5$$

$$R_{\text{top},l} = \frac{(10+4.5) \times 10^{-2}}{1000 \mu_0 \times 4 \times 10^{-4}}$$

$$R_{\text{bot},l} = \frac{(10+4.5) \times 10^{-2}}{1000 \mu_0 \times 4 \times 10^{-4}}$$

$$R_{\text{top},r} = R_{\text{bot},r} = \frac{(10+4.75) \times 10^{-2}}{1000 \mu_0 \times 4 \times 10^{-4}}$$

$$R_{\text{gap},l} = \frac{10^{-2}}{\mu_0 ([2+1] \times [2+1]) \times 10^{-4}}$$

add length of gap to each dimension to account for fringing

$$R_{\text{gap},r} = \frac{0.5 \times 10^{-2}}{\mu_0 ([2+0.5] \times [2+0.5]) \times 10^{-4}}$$

Now combine reluctances in series



$$R_c = R_{top,l} + R_{gap,l} + R_{bot,l} = 9.42 \times 10^6$$

$$R_r = R_{top,r} + R_{gap,r} + R_{bot,r} = 6.953 \times 10^6$$

$$R_e = 1.989 \times 10^5$$

Redraw



⇒ solve for ϕ 's using current division ideas

$$\text{Total reluctance, } R_t = R_e + \frac{1}{\frac{1}{R_L} + \frac{1}{R_R}}$$

$$= 4.199 \times 10^6$$

$$\Rightarrow \phi_c = F/R_t = 238.1 \mu\text{Wb}$$

$$\text{Flux division } \phi_L = \phi_c \frac{R_R}{R_L + R_R} = 101.1 \mu\text{Wb}$$

$$\phi_R = \phi_c \frac{R_L}{R_L + R_R} = 137.0 \mu\text{Wb}$$

$$B_{\text{gap},e} = \frac{\phi_e}{([2+1] \times [2+1]) \times 10^{-4}} = 0.1123 \text{ T}$$

$$B_{\text{gap},r} = \frac{\phi_r}{([2+0.5] \times [2+0.5]) \times 10^{-4}} = 0.2192 \text{ T}$$

NOTES

- Core reluctances usually small with respect to gaps.
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