## EE 4CL4 – Control System Design

## Solutions to Homework Assignment #4

1. The input-output model for a system is given by:

$$\ddot{y}(t) + 7\dot{y}(t) + 12y(t) = 3u(t)$$
, where  $\ddot{y}(t) = \frac{d^2 y(t)}{dt^2}$  and  $\dot{y}(t) = \frac{d y(t)}{dt}$ .

- a. Determine the system transfer function.
- b. Compute the unit step response with zero initial conditions.
- c. Repeat with initial conditions y(0) = -1 and  $\dot{y}(0) = 2$ . (25 pts)
- a. The system transfer function H(s) can be determined by taking the Laplace transform of the differential equation with zero initial conditions:

$$\mathcal{L}[\ddot{y}(t) + 7\dot{y}(t) + 12y(t) = 3u(t)] = s^{2}Y(s) - sy(0) - \dot{y}(0) + 7(sY(s) - y(0)) + 12Y(s) = 3U(s),$$
  
$$\Rightarrow H(s) = \frac{Y(s)}{U(s)} = \frac{3}{s^{2} + 7s + 12} = \frac{3}{(s+3)(s+4)}.$$

b. To compute the unit step response y(t) with zero initial conditions, we compute the inverse Laplace transform for Y(s)=H(s)U(s)=H(s)/s, giving:

$$y(t) = \frac{1}{4} - e^{-3t} + \frac{3}{4}e^{-4t}$$
.

c. To compute the unit step response y(t) with initial conditions y(0) = -1 and  $\dot{y}(0) = 2$ , we can compute the Laplace transform as for part a., but including the values for the initial conditions. The inverse Laplace transform of Y(s) can then be calculated for U(s)=1/s, giving:

$$s^{2}Y(s) + s - 2 + 7(sY(s) + 1) + 12Y(s) = 3U(s) \Longrightarrow Y(s) = \frac{-s^{2} - 5s + 3}{s(s+3)(s+4)},$$
$$y(t) = \frac{1}{4} - 3e^{-3t} + \frac{7}{4}e^{-4t}.$$

A different approach is to use the result from part b. where we have computed the system's natural modes. The new output has the general form:

$$y(t) = \frac{1}{4} + K_1 e^{-3t} + K_2 e^{-4t}$$
,

where the constants  $K_1$  and  $K_2$  are chosen to satisfy the initial conditions, i.e.:

$$y(0) = -1 = \frac{1}{4} + K_1 + K_2$$
 and  $\dot{y}(0) = 2 = -3K_1 - 4K_2$ .

The above equations are satisfied for  $K_1 = -3$ ,  $K_2 = 7/4$ .

2. Analyze, for  $\beta \in \Re$ , the frequency response of the AME and the MME when the true and the nominal models are given by:

$$G(s) = \frac{\beta s + 2}{(s+1)(s+2)}$$
 and  $G_o(s) = \frac{2}{(s+1)(s+2)}$ ,

respectively.

Is the AME low-pass, band-pass or high-pass? What about the MME? (25 pts)

From the given equations, the AME is:

$$G_{\epsilon}(s) = G(s) - G_{o}(s) = \frac{\beta s}{(s+1)(s+2)},$$

and the MME is:

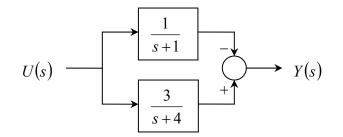
$$G_{\Delta}(s) = \frac{G_{\epsilon}(s)}{G_{o}(s)} = \frac{\beta s}{2}.$$

To obtain the frequency response of the AME and MME we substitute  $s = j\omega$  into the above equations, giving:

$$G_{\epsilon}(j\omega) = \frac{\beta j\omega}{(j\omega+1)(j\omega+2)}$$
 and  $G_{\Delta}(j\omega) = \frac{\beta j\omega}{2}$ .

From these equations it can be seen that the AME is band-pass, while the MME is high-pass.

## 3. A parallel connection of 2 systems is illustrated by the following block diagram:



- a. What is the transfer function from *u* to *y*?
- b. What are the system poles and zero?
- c. Calculate the system step response. How does the system zero influence the shape of the step response? (25 pts)

a. The transfer function H(s) from u to y is:

$$H(s) = \frac{3}{s+4} - \frac{1}{s+1} = \frac{2s-1}{(s+1)(s+4)}.$$

- b. The system poles are the combination of the poles of the individual systems, i.e., s = -1 and s = -4. The system zero is located at s = 0.5, i.e. it is a non-minimum-phase zero.
- c. The step response is given by:

$$y(t) = \mathcal{L}^{-1}[H(s)/s] = \mathcal{L}^{-1}\left[\frac{2s-1}{s(s+1)(s+4)}\right] = -\frac{1}{4}(1-4e^{-t}+3e^{-4t}).$$

The initial movement of y(t) is in the positive direction  $(\dot{y}(0)=2)$ , but the steady state value of y is negative  $(y(t \rightarrow \infty) = -1/4)$ . That is, the non-minimum-phase zero creates an undershoot in the step response.

4. Calculate the steady-state responses when a unit step is applied to the following systems, commenting on the differences observed.

$$G(s) = \frac{1}{s^3 + 3s^2 + 3s + 1}, \text{ (Hint: you will need to use the Laplace-transform property}$$
$$\mathcal{L}[t^k y(t)] = (-1)^k \frac{d^k Y(s)}{ds^k} \text{ for one inverse Laplace}$$
$$transform)$$

$$G(s) = \frac{s^2 + 2s}{s^3 + 3s^2 + 3s + 1}.$$
 (25 pts)

Partial fraction decomposition of Y(s)=G(s)U(s)=G(s)/s for each of the above transfer function gives:

$$Y(s) = \frac{1}{s(s+1)^3} = \frac{1}{s} - \frac{1}{s+1} - \frac{1}{(s+1)^2} - \frac{1}{(s+1)^3} \quad \text{and} \quad Y(s) = \frac{s+2}{(s+1)^3} = \frac{1}{(s+1)^2} + \frac{1}{(s+1)^3},$$

respectively. The inverse Laplace transform of each of these equations is:

 $y(t) = 1 - e^{-t} - t e^{-t} - \frac{1}{2}t^2 e^{-t}$  and  $y(t) = t e^{-t} + \frac{1}{2}t^2 e^{-t}$ ,

respectively. Note that  $\mathcal{L}^{-1}\left[\frac{1}{(s+1)^3}\right] = \mathcal{L}^{-1}\left[\frac{1}{2}(-1)^2 \frac{d^2 F(s)}{ds^2}\right] = \frac{1}{2}t^2 e^{-t}$  if  $F(s) = \frac{1}{s+1}$ .

Alternatively, the steady-state step responses can be calculated via the final value theorem.

The main difference between these two systems lies in the d.c. gains. The second system has a zero at the origin, thus it has zero d.c. gain, and the unit step response vanishes asymptotically.