

ECE 2E14 - Lecture 4

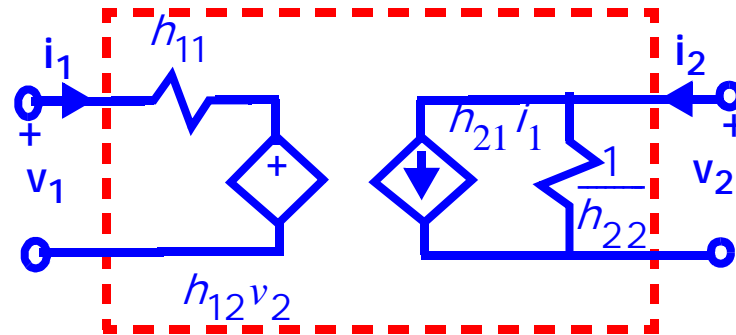
Outline/Learning Objectives:

- Describe the concept of linear amplification (and nonlinear distortion).
- Define the quantities used to measure the performance of analog amplifiers, including voltage gain, current gain, power gain, input and output resistances.
- Express the voltage, current, and power gain in terms of the decibel, or dB.
- Describe amplifier biasing for linear operation.
- Model linear amplifiers using simple two-port representations (g-parameters, h-parameters, y-parameters, and z-parameters).
- Define unilateral two-port representations of linear amplifiers.
- Describe mismatched conditions at the input and output ports of an amplifier and the concepts of ideal voltage and current amplifiers.
- Use the electronics laboratory to investigate the electrical behaviour of simple circuits and devices.
- From Chapter 10 in Jaeger

The Hybrid or h-parameters



$$\begin{bmatrix} v_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \cdot \begin{bmatrix} i_1 \\ v_2 \end{bmatrix}$$



$$\begin{bmatrix} v_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} h_{11}i_1 + h_{12}v_2 \\ h_{21}i_1 + h_{22}v_2 \end{bmatrix}$$

$$h_{11} = \left. \frac{v_1}{i_1} \right|_{v_2=0} \quad \text{SC } R_{in}$$

$$h_{12} = \left. \frac{v_1}{v_2} \right|_{i_1=0} \quad \text{Reverse OC V-gain}$$

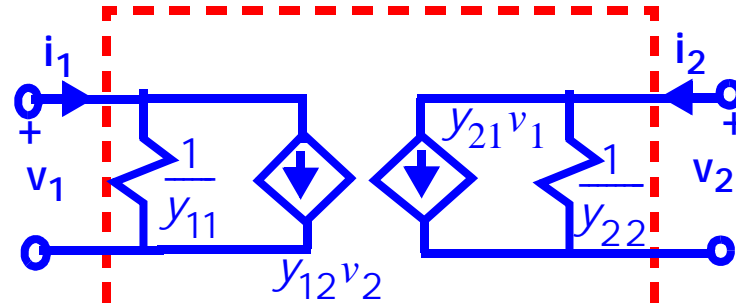
$$h_{21} = \left. \frac{i_2}{i_1} \right|_{v_2=0} \quad \text{Forward SC I-gain}$$

$$h_{22} = \left. \frac{i_2}{v_2} \right|_{i_1=0} \quad \text{OC } G_{out}$$

The Admittance or y-parameters



$$\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \cdot \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$



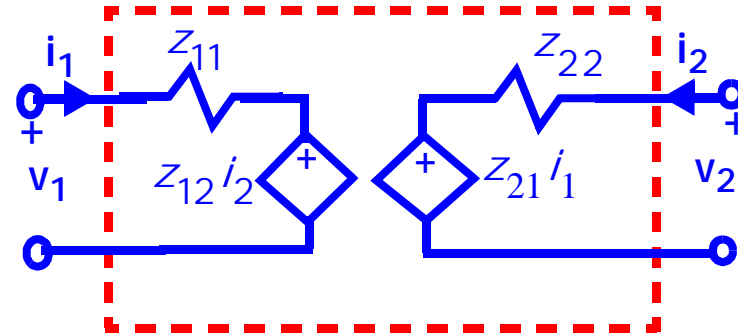
$$\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} y_{11}v_1 + y_{12}v_2 \\ y_{21}v_1 + y_{22}v_2 \end{bmatrix}$$

$$y_{11} = \left. \frac{i_1}{v_1} \right|_{v_2=0} \quad \text{SC } G_{in}$$

$$y_{12} = \left. \frac{i_1}{v_2} \right|_{v_1=0} \quad \text{Reverse SC trans-G}$$

$$y_{21} = \left. \frac{i_2}{v_1} \right|_{v_2=0} \quad \text{Forward SC trans-G} \quad y_{22} = \left. \frac{i_2}{v_2} \right|_{v_1=0} \quad \text{SC } G_{out}$$

The Impedance or z-parameters



$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} z_{11} & z_{12} \\ z_{21} & z_{22} \end{bmatrix} \cdot \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$$

$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} z_{11}i_1 + z_{12}i_2 \\ z_{21}i_1 + z_{22}i_2 \end{bmatrix}$$

$$z_{11} = \left. \frac{v_1}{i_1} \right|_{i_2=0} \quad \text{OC } R_{in}$$

$$z_{12} = \left. \frac{v_1}{i_2} \right|_{i_1=0} \quad \text{Reverse OC trans-R}$$

$$z_{21} = \left. \frac{v_2}{i_1} \right|_{i_2=0} \quad \text{Forward OC trans-R}$$

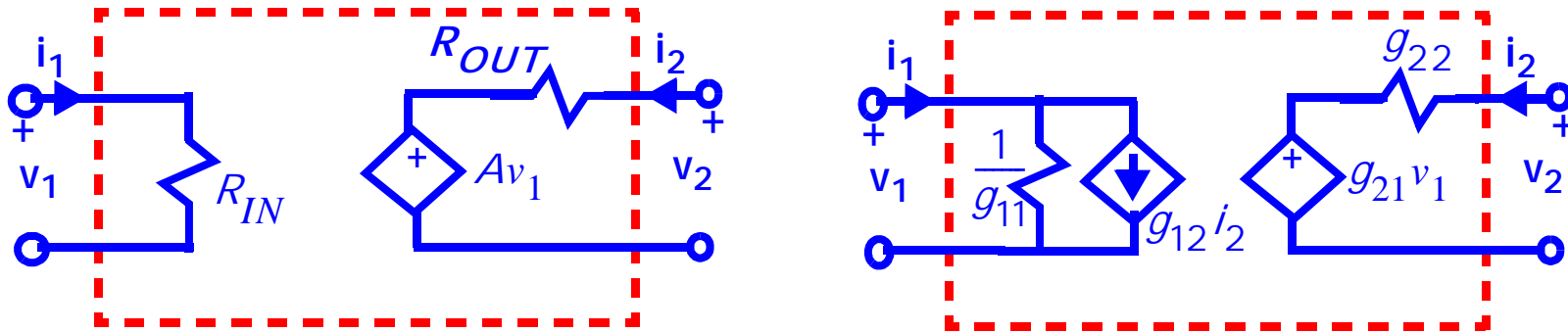
$$z_{22} = \left. \frac{v_2}{i_2} \right|_{i_1=0} \quad \text{OC } R_{out}$$

Mismatched Source and Load Resistances

Assume that forward voltage or current gain, or transconductance or transresistance is much larger than corresponding reverse parameter.

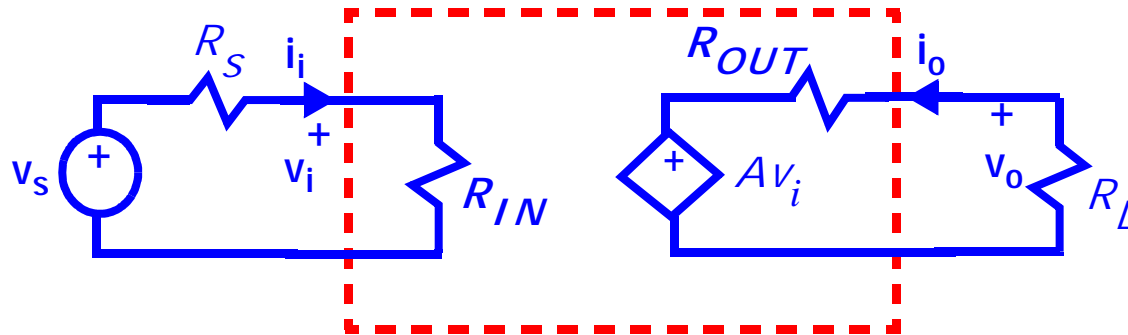
For example, $g_{21} \gg g_{12}$ or $y_{21} \gg y_{12}$.

Two-port g-parameters representation of voltage amplifier



Here, $R_{IN} = (1/g_{11})$, $g_{12} = 0$, $A = g_{21}$ and $R_{OUT} = g_{22}$

Voltage Amplifiers



Here, $v_o = Av_i \cdot \frac{R_L}{R_{OUT} + R_L}$ and $v_i = v_s \cdot \frac{R_{IN}}{R_{IN} + R_S}$. Note $v_s = v_i \cdot \frac{R_{IN} + R_S}{R_{IN}}$

Therefore, $|A_V| = \frac{V_o}{V_s} = A \cdot \frac{R_L}{R_{OUT} + R_L} \cdot \frac{R_{IN}}{R_{IN} + R_S}$.

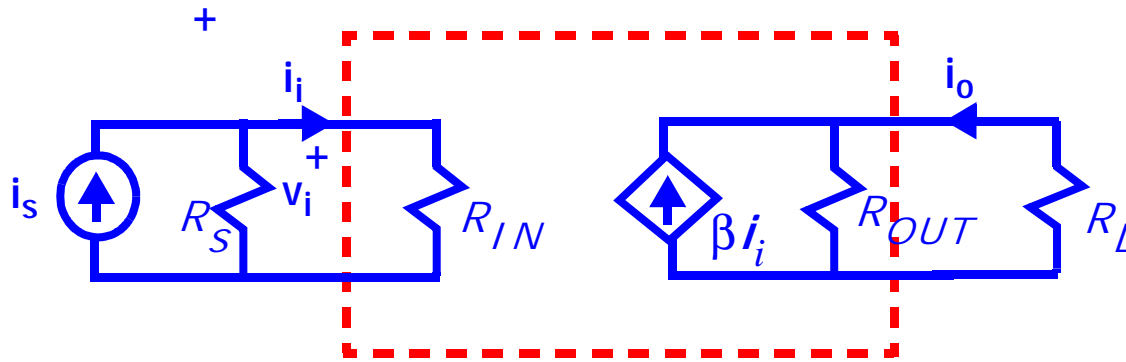
To achieve maximum gain, require $R_{IN} \gg R_S$ and $R_{OUT} \ll R_L$.

In ideal voltage amplifier, $R_{IN} = \infty$ and $R_{OUT} = 0 \Rightarrow |A_V| = A$.

Current gain, $|A_I| = \frac{I_o}{I_s} = \frac{V_o/R_L}{V_s/(R_{IN} + R_S)} = \frac{V_o}{V_s} \cdot \frac{R_{IN} + R_S}{R_L}$.

Can also write as $|A_I| = |A_V| \cdot \frac{R_{IN} + R_S}{R_L}$

Current Amplifiers



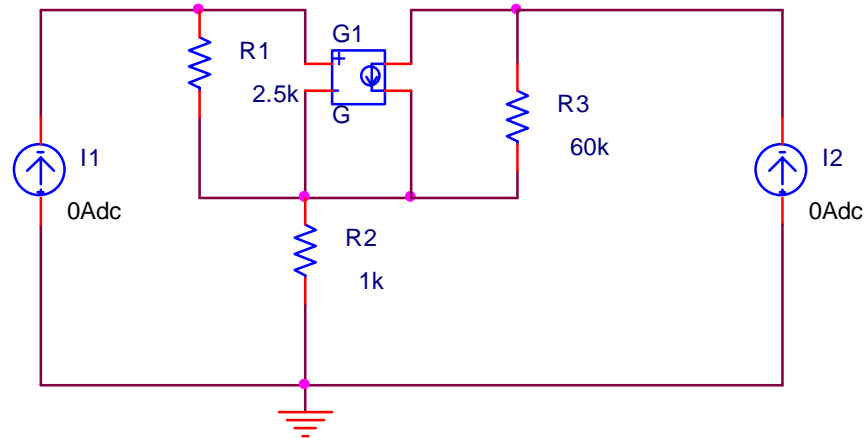
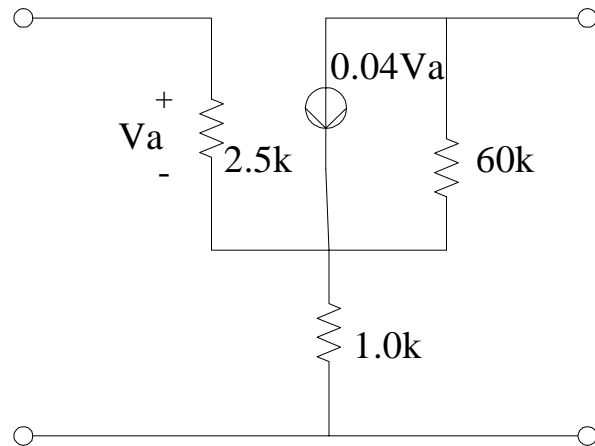
Now, $i_o = \beta i_i \cdot \frac{R_{OUT}}{R_{OUT} + R_L}$ and $i_i = i_s \cdot \frac{R_S}{R_S + R_{IN}}$. Note $i_s = i_i \cdot \frac{R_S + R_{IN}}{R_S}$

Therefore, $|A_I| = \frac{I_o}{I_s} = \beta \cdot \frac{R_{OUT}}{R_{OUT} + R_L} \cdot \frac{R_S}{R_S + R_{IN}}$.

To achieve maximum gain, require $R_S \gg R_{IN}$ & $R_{OUT} \gg R_L \Rightarrow |A_I| = \beta$

Ideal Current Amplifier has $R_{IN} = 0$ and $R_{OUT} = \infty$.

PSPI CE EXAMPLE



*Libraries:

* Local Libraries :

* From [PSPICE NETLIST] section of C:\Program Files\OrcadLite\PSpice\PSpice.ini file:

.lib "nom.lib"

*Analysis directives:

.TF V([N00191]) I_I1

.PROBE V(*) I(*) W(*) D(*) NOISE(*)

.INC ".\example1-SCHEMATIC1.net"

**** INCLUDING example1-SCHEMATIC1.net ****

* source EXAMPLE1

R_R1 N00025 N00153 2.5k

R_R3 N00025 N00191 60k

R_R2 0 N00025 1k

I_I1 0 N00153 DC 0Adc

G_G1 N00191 N00025 N00153 N00025 0.04

I_I2 0 N00191 DC 0Adc

.END

PSPI CE EXAMPLE (Cont'd)

**** SMALL-SIGNAL CHARACTERISTICS

$V(N00191)/I_{I1} = -5.999E+06$

INPUT RESISTANCE AT $I_{I1} = 3.500E+03$

OUTPUT RESISTANCE AT $V(N00191) = 6.100E+04$

Z parameters are $Z_{11}=3.5K$, $Z_{21}=-6M$, $Z_{12}=1K$, $Z_{22}=61K$