

EE750
Advanced Engineering Electromagnetics
Lecture 12

Duality

- Duality means that two differential/integral equations describing the behavior of two different variables have the same mathematical forms \implies solutions are identical
- Equations describing the case ($\mathbf{J} \neq \mathbf{0}$, $\mathbf{M} = \mathbf{0}$) are dual to equations describing the case ($\mathbf{J} = \mathbf{0}$, $\mathbf{M} \neq \mathbf{0}$)

$$\begin{aligned}\nabla \times \mathbf{E}_A &= -j\omega\mu \mathbf{H}_A \\ \nabla \times \mathbf{H}_A &= \mathbf{J} + j\omega\epsilon \mathbf{E}_A \\ \nabla^2 \mathbf{A} + \beta^2 \mathbf{A} &= -\mu\mathbf{J} \\ \mathbf{A} &= \frac{\mu}{4\pi} \iiint_{V'} \frac{\mathbf{J}}{R} e^{-j\beta R} dV'\end{aligned}$$

$$\begin{aligned}\nabla \times \mathbf{H}_F &= j\omega\epsilon \mathbf{E}_F \\ \nabla \times \mathbf{E}_F &= -\mathbf{M} - j\omega\mu \mathbf{H}_F \\ \nabla^2 \mathbf{F} + \beta^2 \mathbf{F} &= -\epsilon\mathbf{M} \\ \mathbf{F} &= \frac{\epsilon}{4\pi} \iiint_{V'} \frac{\mathbf{M}}{R} e^{-j\beta R} dV'\end{aligned}$$

Duality (Cont'd)

$$\begin{array}{l} \mathbf{H}_A = (1/\mu)\nabla \times \mathbf{A} \\ \mathbf{E}_A = -j\omega\mathbf{A} - (j/\omega\mu\epsilon)(\nabla(\nabla \cdot \mathbf{A})) \end{array} \left\| \begin{array}{l} \mathbf{E}_F = (-1/\epsilon)\nabla \times \mathbf{F} \\ \mathbf{H}_F = -j\omega\mathbf{F} - (j/\omega\mu\epsilon)(\nabla(\nabla \cdot \mathbf{F})) \end{array} \right.$$

It follows that the following quantities are identical

$$\mathbf{E}_A \iff \mathbf{H}_F \quad \mathbf{H}_A \iff -\mathbf{E}_F \quad \mathbf{J} \iff \mathbf{M}$$

$$\mathbf{A} \iff \mathbf{F} \quad \epsilon \iff \mu \quad \mu \iff \epsilon$$

$$\beta \iff \beta \quad \eta \iff 1/\eta$$

Example

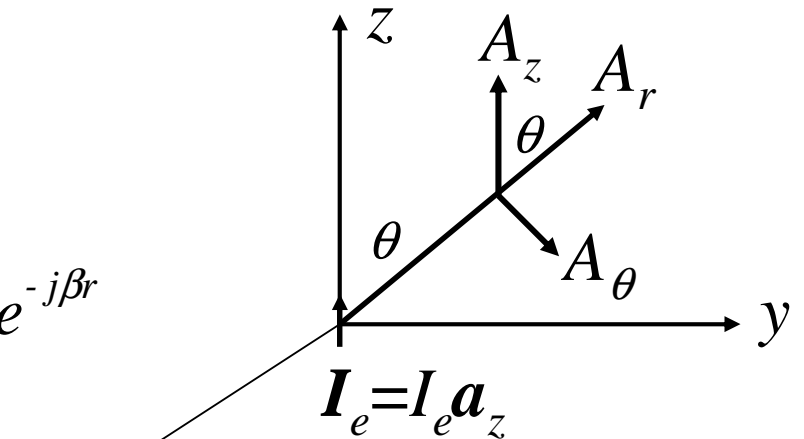
Using Duality, find the fields resulting from an infinitesimal magnetic dipole $\mathbf{I}_m = \mathbf{a}_z I_m$

The fields resulting from an electric dipole are

$$E_r = \frac{\eta I_e l}{2\pi r^2} \cos\theta \left(1 + \frac{1}{j\beta r}\right) e^{-j\beta r}$$

$$E_\theta = \frac{j\eta\beta I_e l}{4\pi r} \sin\theta \left(1 + \frac{1}{j\beta r} - \frac{1}{(\beta r)^2}\right) e^{-j\beta r}$$

$$H_\phi = \frac{j\beta I_e l}{4\pi r} \sin\theta \left(1 + \frac{1}{j\beta r}\right) e^{-j\beta r}$$



Example (Cont'd)

It follows that the fields resulting from the magnetic dipole are given by

$$H_r = \frac{I_m l}{2\eta\pi r^2} \cos\theta \left(1 + \frac{1}{j\beta r}\right) e^{-j\beta r}$$

$$H_\theta = \frac{j\beta I_m l}{4\eta\pi r} \sin\theta \left(1 + \frac{1}{j\beta r} - \frac{1}{(\beta r)^2}\right) e^{-j\beta r}$$

$$E_\phi = \frac{-j\beta I_m l}{4\pi r} \sin\theta \left(1 + \frac{1}{j\beta r}\right) e^{-j\beta r}$$

Uniqueness Theorem

- This theorem establishes the conditions under which a unique solution exists for a given problem
- Assume that a closed surface S encloses a material with sources $\mathbf{J}_i, \mathbf{M}_i$ and complex parameters $\epsilon = \epsilon' - j\epsilon''$,
 $\mu = \mu' - j\mu''$
- If there are two possible solutions $\mathbf{E}^a, \mathbf{H}^a$ and $\mathbf{E}^b, \mathbf{H}^b$, they must satisfy Maxwell's equations

$$\nabla \times \mathbf{E}^a = -\mathbf{M}_i - j\omega\mu \mathbf{H}^a \quad , \quad \nabla \times \mathbf{H}^a = \mathbf{J}_i + \sigma \mathbf{E}^a + j\omega\epsilon \mathbf{E}^a$$

$$\nabla \times \mathbf{E}^b = -\mathbf{M}_i - j\omega\mu \mathbf{H}^b \quad , \quad \nabla \times \mathbf{H}^b = \mathbf{J}_i + \sigma \mathbf{E}^b + j\omega\epsilon \mathbf{E}^b$$

Uniqueness Theorem (Cont'd)

- Subtracting the corresponding equations we get

$$\nabla \times \delta \mathbf{E} = -j\omega\mu\delta \mathbf{H} \quad , \quad \nabla \times \delta \mathbf{H} = (\sigma + j\omega\epsilon)\delta \mathbf{E}$$

where $\delta \mathbf{E} = \mathbf{E}^a - \mathbf{E}^b$ and $\delta \mathbf{H} = \mathbf{H}^a - \mathbf{H}^b$

- Notice that the differential fields satisfy the source-free Maxwell's equations
- Applying the source-free conservation of energy relation for $\delta \mathbf{E}$ and $\delta \mathbf{H}$ we get

$$\oint_S (\delta \mathbf{E} \times \delta \mathbf{H}^*) \cdot d\mathbf{s} = -\iiint_V \left[\delta \mathbf{E} \cdot (\sigma + j\omega\epsilon) \delta \mathbf{E}^* + \delta \mathbf{H}^* \cdot (j\omega\mu) \delta \mathbf{H} \right] dv$$

$$\begin{aligned} \oint_S (\delta \mathbf{E} \times \delta \mathbf{H}^*) \cdot d\mathbf{s} &= -\iiint_V \left((\sigma + \omega\epsilon'') |\delta \mathbf{E}|^2 + \omega\mu'' |\delta \mathbf{H}|^2 \right) dv \\ &\quad - j\iiint_V \left(-\omega\epsilon' |\delta \mathbf{E}|^2 + \omega\mu' |\delta \mathbf{H}|^2 \right) dv \end{aligned}$$

Uniqueness Theorem (Cont'd)

- Now if we have $\oiint_S (\delta \mathbf{E} \times \delta \mathbf{H}^*) \cdot d\mathbf{s} = 0$, this implies that $\delta \mathbf{E} = \delta \mathbf{H} = \mathbf{0}$ everywhere inside S . Notice that the assumption of losses existence is important!
- Using the vector identity $\mathbf{A} \cdot \mathbf{B} \times \mathbf{C} = \mathbf{B} \cdot \mathbf{C} \times \mathbf{A} = \mathbf{C} \cdot \mathbf{A} \times \mathbf{B}$, we have
$$\oiint_S (\delta \mathbf{E} \times \delta \mathbf{H}^*) \cdot d\mathbf{s} \mathbf{n} = \oiint_S (\mathbf{n} \times \delta \mathbf{E}) \cdot \delta \mathbf{H}^* ds = \oiint_S (\delta \mathbf{H}^* \times \mathbf{n}) \cdot \delta \mathbf{E} ds$$
- It follows that the condition $\oiint_S (\delta \mathbf{E} \times \delta \mathbf{H}^*) \cdot d\mathbf{s} = 0$ implies that one of the following three cases is satisfied:
 - a) The tangential component of the \mathbf{E} field is specified on S , i.e. $\mathbf{n} \times \delta \mathbf{E} = \mathbf{0}$ on S

Uniqueness Theorem (Cont'd)

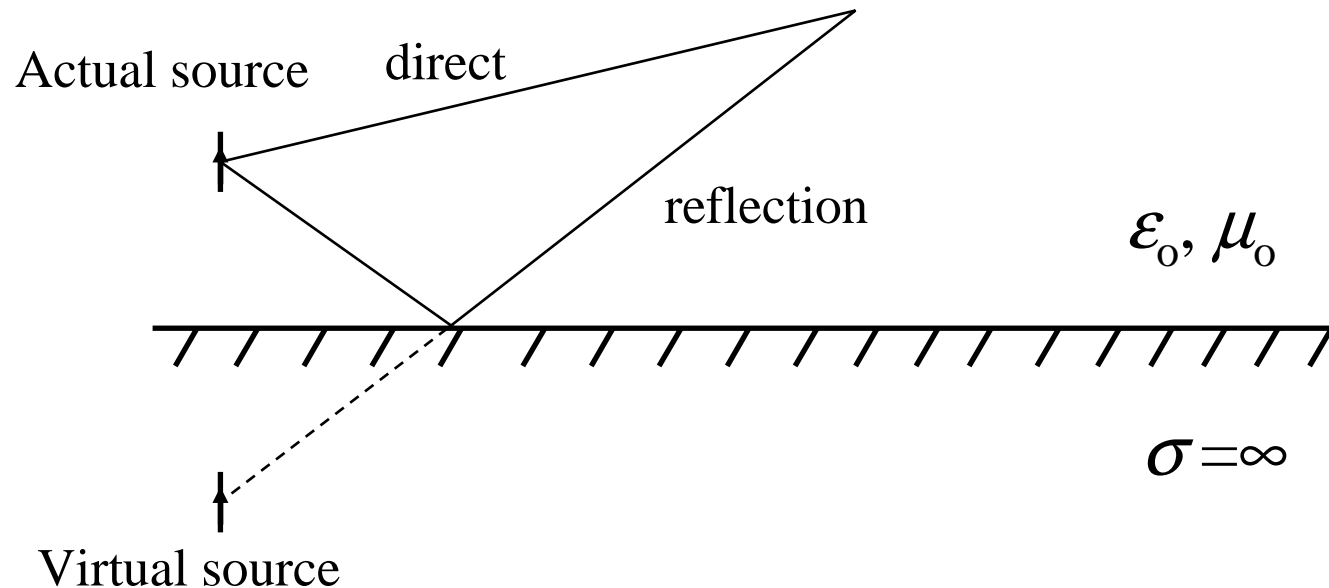
- b) The tangential component of the \mathbf{H} field is specified on S ,
i.e. $\mathbf{n} \times \delta \mathbf{H} = \mathbf{0}$ on $S \implies \delta \mathbf{H}^* \times \mathbf{n} = \mathbf{0}$ on S
- c) The tangential component of the \mathbf{E} field is specified on part of S and the tangential component of the \mathbf{H} field is specified on the rest of S , i.e.

$$\mathbf{n} \times \delta \mathbf{E} = \mathbf{0} \text{ on } S_1$$

$$\mathbf{n} \times \delta \mathbf{H} = \mathbf{0} \text{ on } S_2$$

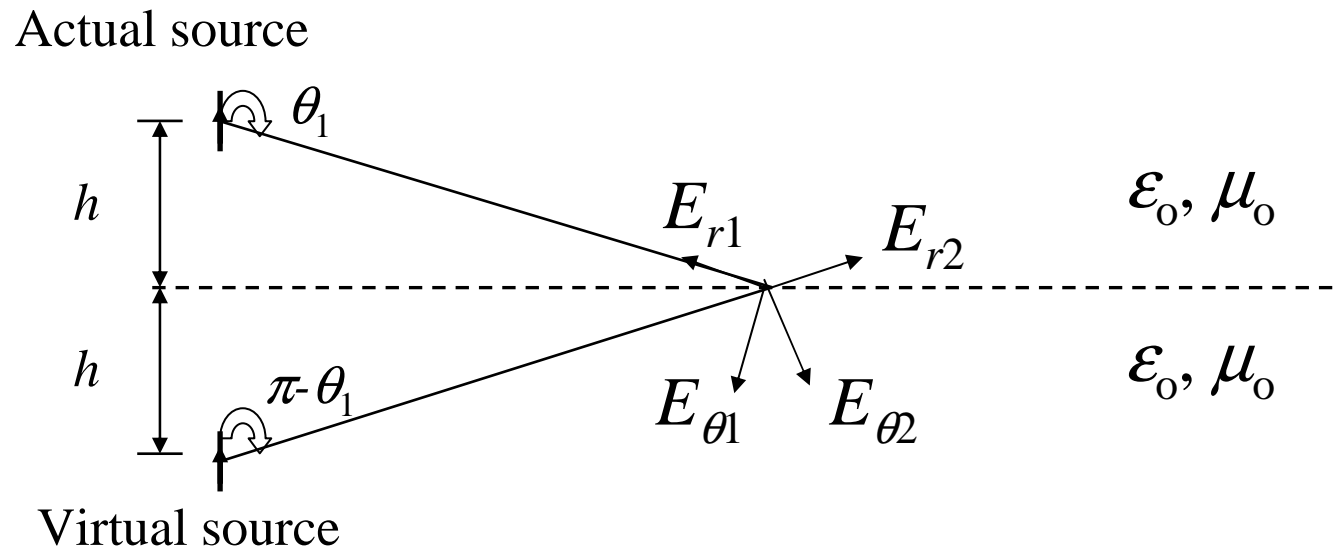
$$S = S_1 \cup S_2$$

Image Theory



- Image theory enables us to evaluate the field generated by sources placed near infinite perfectly conducting boundary
- Virtual sources are added to maintain the same tangential field boundary conditions for the original problem

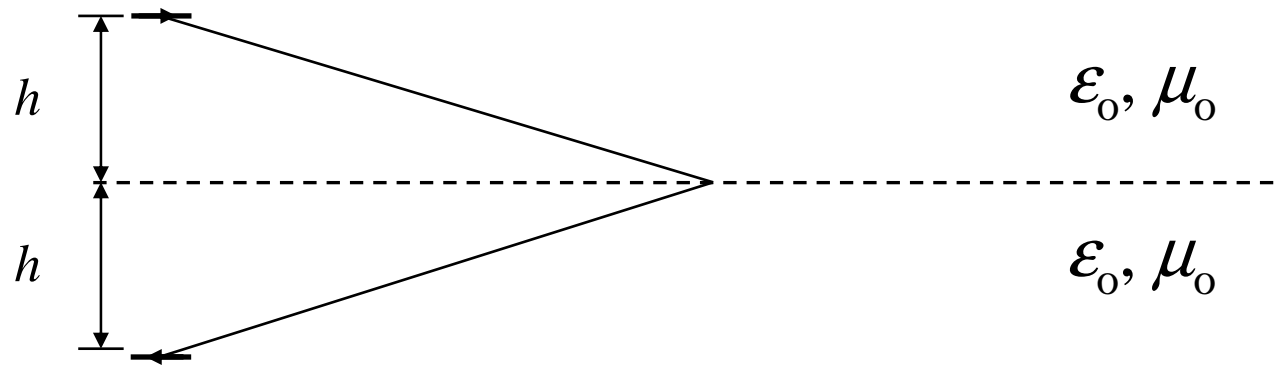
Image Theory (Cont'd)



- Image of a vertical electric dipole is another vertical electric dipole (same orientation)
- Notice that the tangential electric field components cancel out

Image Theory (Cont'd)

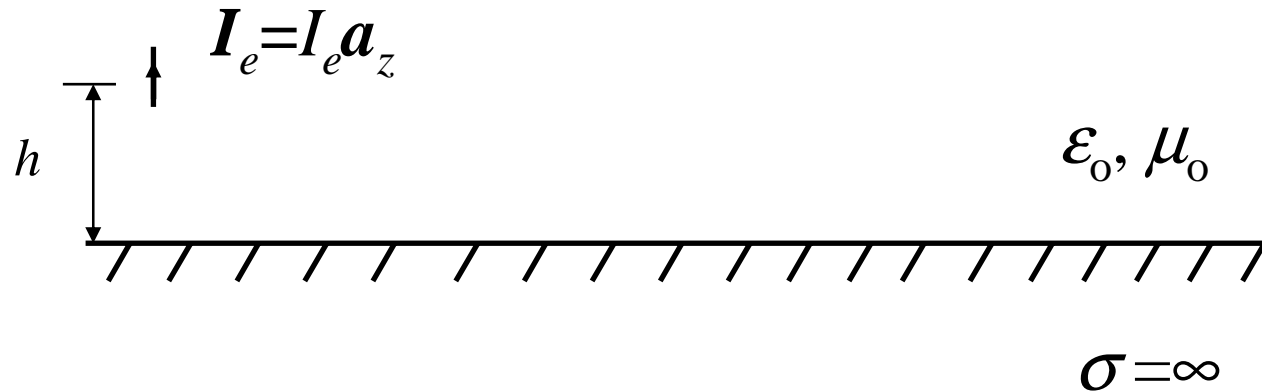
Actual source



Virtual source

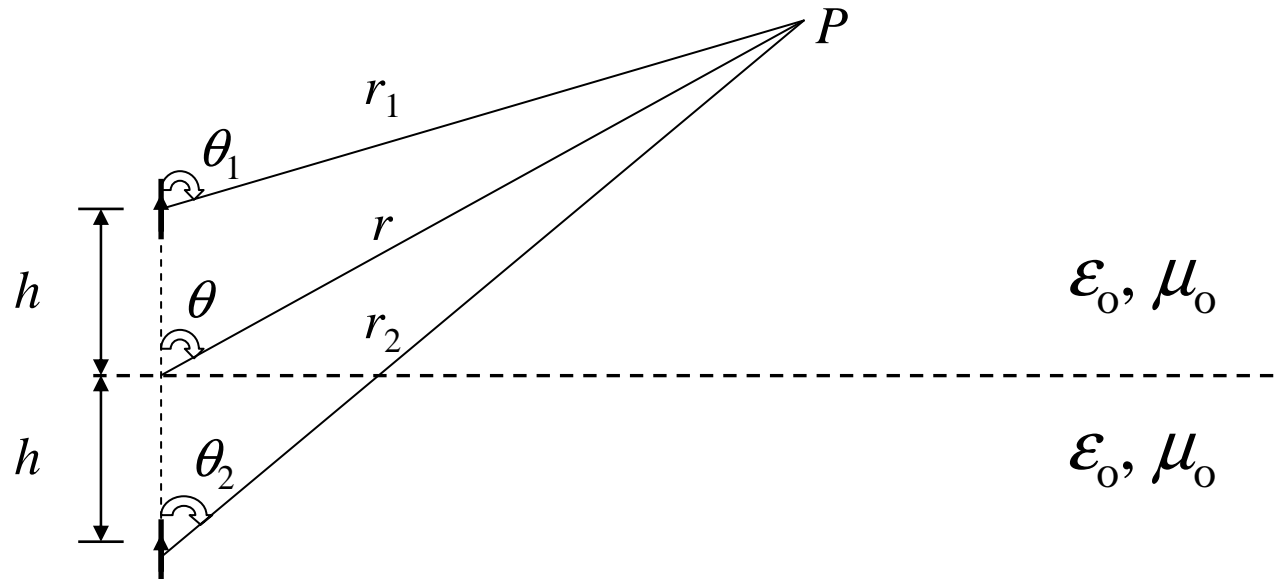
Image for a horizontal electric dipole has the same value but opposite orientation (Prove it!)

Example



- Obtain an expression for the far fields generated by a vertical electric dipole of length l placed near an infinite conducting wall

Example (Cont'd)



For the far fields we have

$$E_{\theta}^1 = \frac{j\eta\beta I_e l}{4\pi r_1} \sin\theta_1 e^{-j\beta r_1} \quad \text{and} \quad E_{\theta}^2 = \frac{j\eta\beta I_e l}{4\pi r_2} \sin\theta_2 e^{-j\beta r_2}$$

$$\begin{aligned} r_1^2 &= r^2 + h^2 - 2rh \cos\theta \\ r_2^2 &= r^2 + h^2 + 2rh \cos\theta \end{aligned} \quad \begin{array}{c} r \gg h \\ \longrightarrow \end{array} \quad \begin{aligned} r_1 &= r - h \cos\theta \\ r_2 &= r + h \cos\theta \end{aligned}$$

Example (Cont'd)

- Further, we can use for the amplitude $r=r_1=r_2$
- The total field in the top half space is the sum of the field generated by both the actual and virtual sources

$$E_{\theta} = E_{\theta}^1 + E_{\theta}^2 = \frac{j\eta\beta I_e l}{4\pi r} \sin \theta e^{-j\beta r} (e^{j\beta h \cos \theta} + e^{-j\beta h \cos \theta})$$

$z \geq 0$

$$E_{\theta}=0, \quad z < 0$$

- Combining terms we get

$$E_{\theta} = \underbrace{\frac{j2\eta\beta I_e l}{4\pi r} \sin \theta e^{-j\beta r}}_{\text{element factor}} \underbrace{\cos(\beta h \cos \theta)}_{\text{array factor}}$$

Reciprocity Theorem

- Reciprocity theorem in circuit theory states that we can change the location of the source and observation points without affecting the measured values
- A similar theorem can be derived for electromagnetics
- Assume that two sets of sources $\mathbf{J}_1, \mathbf{M}_1$ and $\mathbf{J}_2, \mathbf{M}_2$ radiate within a linear isotropic medium
- Using Maxwell's equations, we have

$$\left. \begin{aligned} \nabla \times \mathbf{E}_1 &= -\mathbf{M}_1 - j\omega\mu \mathbf{H}_1 \\ \nabla \times \mathbf{H}_1 &= \mathbf{J}_1 + j\omega\epsilon \mathbf{E}_1 \end{aligned} \right| \begin{aligned} \nabla \times \mathbf{E}_2 &= -\mathbf{M}_2 - j\omega\mu \mathbf{H}_2 \\ \nabla \times \mathbf{H}_2 &= \mathbf{J}_2 + j\omega\epsilon \mathbf{E}_2 \end{aligned}$$

Reciprocity Theorem (Cont'd)

- Dot multiplying the \mathbf{H}_2 curl equation by \mathbf{E}_1 and dot multiplying the \mathbf{E}_1 curl equation by \mathbf{H}_2 and subtracting we get

$$\mathbf{E}_1 \cdot \nabla \times \mathbf{H}_2 - \mathbf{H}_2 \cdot \nabla \times \mathbf{E}_1 = \mathbf{E}_1 \cdot \mathbf{J}_2 + \mathbf{H}_2 \cdot \mathbf{M}_1 + j\omega\epsilon \mathbf{E}_1 \cdot \mathbf{E}_2 + j\omega\mu \mathbf{H}_1 \cdot \mathbf{H}_2$$



$$-\nabla \cdot (\mathbf{E}_1 \times \mathbf{H}_2) = \mathbf{E}_1 \cdot \mathbf{J}_2 + \mathbf{H}_2 \cdot \mathbf{M}_1 + j\omega\epsilon \mathbf{E}_1 \cdot \mathbf{E}_2 + j\omega\mu \mathbf{H}_1 \cdot \mathbf{H}_2$$

- Similarly, we obtain

$$-\nabla \cdot (\mathbf{E}_2 \times \mathbf{H}_1) = \mathbf{E}_2 \cdot \mathbf{J}_1 + \mathbf{H}_1 \cdot \mathbf{M}_2 + j\omega\epsilon \mathbf{E}_2 \cdot \mathbf{E}_1 + j\omega\mu \mathbf{H}_2 \cdot \mathbf{H}_1$$

- Subtracting these two expressions, we obtain

$$-\nabla \cdot (\mathbf{E}_1 \times \mathbf{H}_2 - \mathbf{E}_2 \times \mathbf{H}_1) = \mathbf{E}_1 \cdot \mathbf{J}_2 + \mathbf{H}_2 \cdot \mathbf{M}_1 - \mathbf{E}_2 \cdot \mathbf{J}_1 - \mathbf{H}_1 \cdot \mathbf{M}_2$$

Reciprocity Theorem (Cont'd)

- Applying divergence theorem, we obtain the Lorentz reciprocity theorem

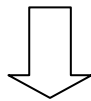
$$-\oint_S (\mathbf{E}_1 \times \mathbf{H}_2 - \mathbf{E}_2 \times \mathbf{H}_1) \cdot d\mathbf{s} = \iiint_V (\mathbf{E}_1 \cdot \mathbf{J}_2 + \mathbf{H}_2 \cdot \mathbf{M}_1 - \mathbf{E}_2 \cdot \mathbf{J}_1 - \mathbf{H}_1 \cdot \mathbf{M}_2) dV$$

- For a source-free region we have

$$-\oint_S (\mathbf{E}_1 \times \mathbf{H}_2 - \mathbf{E}_2 \times \mathbf{H}_1) \cdot d\mathbf{s} = 0$$

- If S is taken as a sphere of infinite radius, we have

$$\iiint_V (\mathbf{E}_1 \cdot \mathbf{J}_2 + \mathbf{H}_2 \cdot \mathbf{M}_1 - \mathbf{E}_2 \cdot \mathbf{J}_1 - \mathbf{H}_1 \cdot \mathbf{M}_2) dV = 0$$

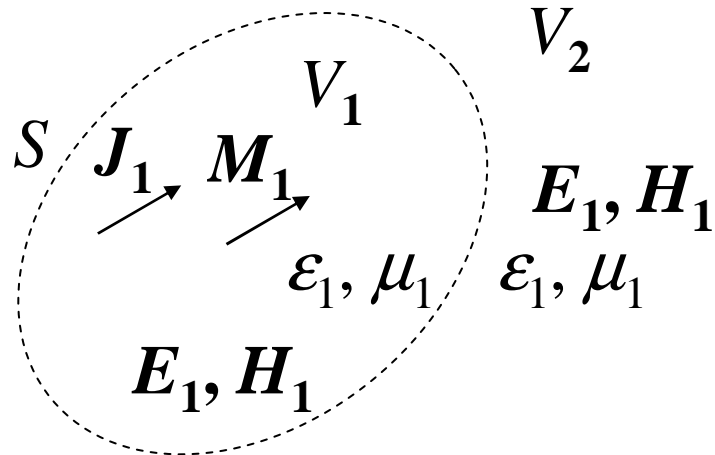


$$\iiint_V (\mathbf{E}_1 \cdot \mathbf{J}_2 - \mathbf{H}_1 \cdot \mathbf{M}_2) dV = \iiint_V (\mathbf{E}_2 \cdot \mathbf{J}_1 - \mathbf{H}_2 \cdot \mathbf{M}_1) dV$$

Surface Equivalence Theorem

- This theorem is based on the uniqueness theorem
- It obtains the fields outside an imaginary surface by placing electric and magnetic sources on the boundary so that the same boundary conditions are satisfied
- Assume that sources \mathbf{J}_1 and \mathbf{M}_1 radiate in an unbounded medium
- We place a virtual surface S that encloses these sources

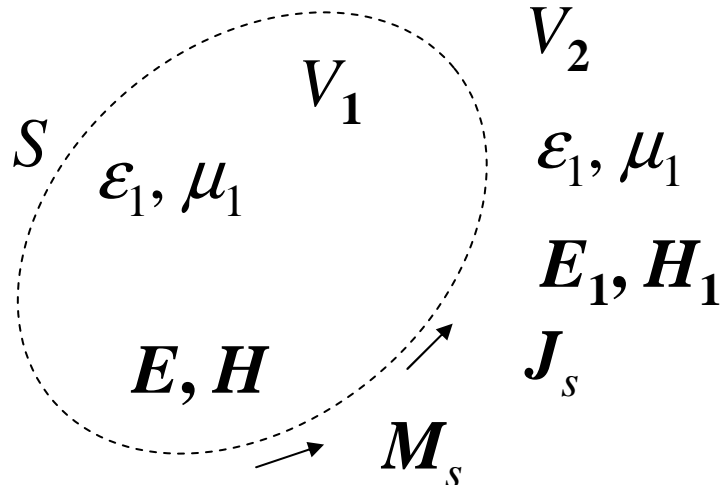
Surface Equivalence Theorem (Cont'd)



Remove the sources and assume arbitrary fields \mathbf{E} , \mathbf{H} inside S . For the boundary conditions to be satisfied we add the boundary sources

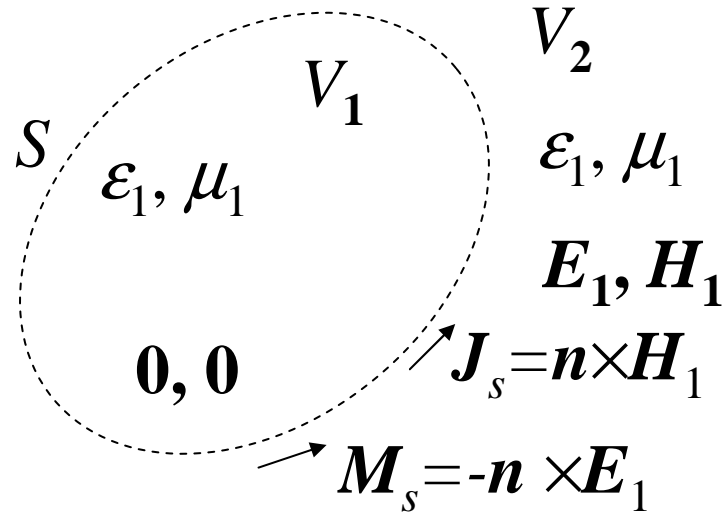
$$\mathbf{J}_s = \mathbf{n} \times (\mathbf{H}_1 - \mathbf{H})$$

$$\mathbf{M}_s = -\mathbf{n} \times (\mathbf{E}_1 - \mathbf{E})$$

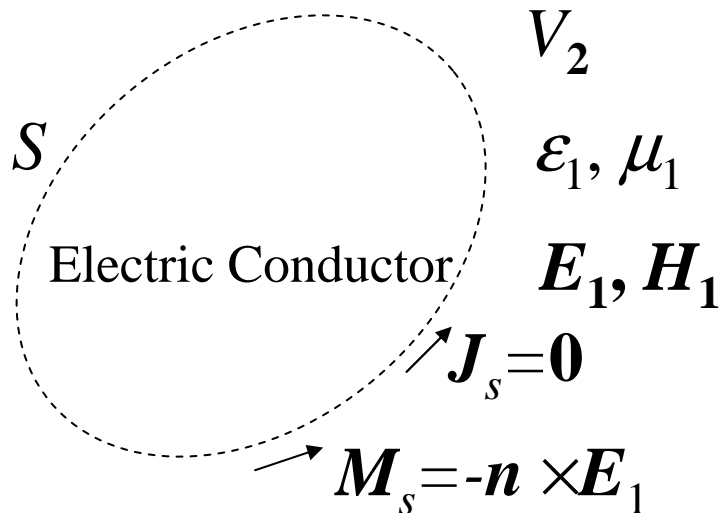


As \mathbf{E} and \mathbf{H} are chosen arbitrarily we may choose $\mathbf{E} = \mathbf{0}$, $\mathbf{H} = \mathbf{0}$

Surface Equivalence Theorem (Cont'd)

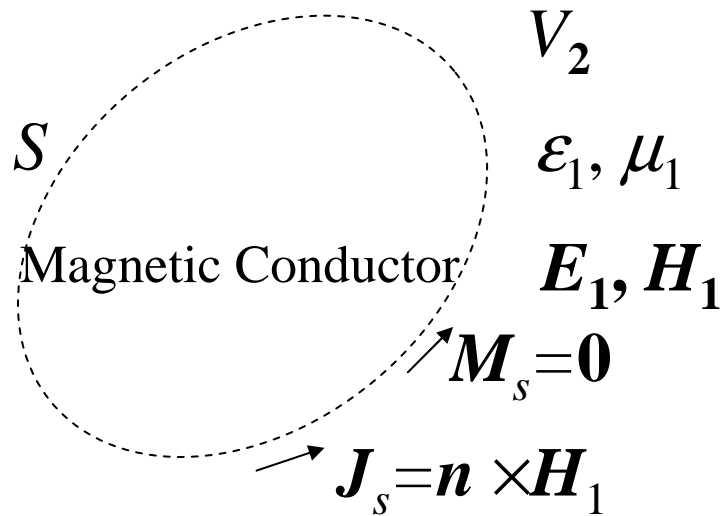


As \mathbf{J}_s and \mathbf{M}_s represent the tangential components of the \mathbf{H}_1 and \mathbf{E}_1 fields, only one of them is needed according to uniqueness theorem



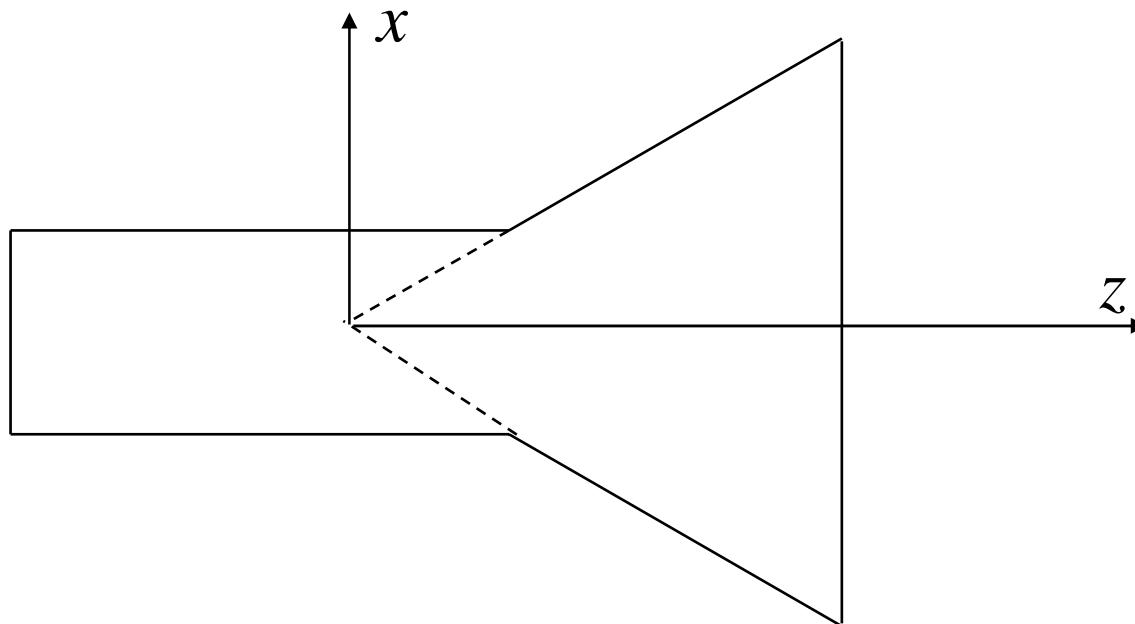
Notice that \mathbf{J}_s is shorted out

Surface Equivalence Theorem (Cont'd)



Notice that M_s is shorted out

Application: H-plan Horn Antenna



- At the surface we know E_y and H_x
- Equivalent sources are given by $J_y = H_x$ and $M_x = E_y$