

a. 8.3) NMP zero at $s = z_0$

From Lemma 8.3: $\int_0^{\infty} e(t) e^{-z_0 t} dt = \frac{1}{z_0}$

$$[0, \infty) = [0, t_1] \cup [t_1, \infty)$$

$$\text{so } \frac{1}{z_0} = \int_0^{t_1} e(t) e^{-z_0 t} dt + \int_{t_1}^{\infty} e(t) e^{-z_0 t} dt$$

since $e(t) \leq |e(t)|$

$$\frac{1}{z_0} \leq \int_0^{t_1} e(t) e^{-z_0 t} dt + \int_{t_1}^{\infty} e(t) e^{-z_0 t} dt$$

$$\leq \int_0^{t_1} |e(t)| e^{-z_0 t} dt + \int_{t_1}^{\infty} |e(t)| e^{-z_0 t} dt$$

since $E_{\max} = \max_{t \in [0, t_1]} (e(t))$ and $|e(t)| \leq e^{-\alpha(t-t_1)}$

$$\leq \int_0^{t_1} E_{\max} e^{-z_0 t} dt + \int_{t_1}^{\infty} e^{-\alpha(t-t_1)} e^{-z_0 t} dt$$

$$\leq E_{\max} \left[-\frac{1}{z_0} e^{-z_0 t} \Big|_0^{t_1} \right] + e^{\alpha t_1} \int_{t_1}^{\infty} e^{-t(\alpha+z_0)} dt$$

$$\frac{1}{z_0} \leq E_{\max} \left[-\frac{1}{z_0} e^{-z_0 t_1} + 1 \right] + \frac{e^{-\alpha t_1}}{\alpha+z_0} \left[e^{-t(\alpha+z_0)} \Big|_{t_1}^{\infty} \right]$$

$$\frac{1}{z_0} \leq E_{\max} \left[\frac{e^{-z_0 t_1}}{z_0} + 1 \right] + \frac{e^{-t_1(\alpha+z_0)}}{\alpha+z_0}$$

$$\frac{1}{z_0} - \frac{e^{-z_0 t_1}}{\alpha+z_0} \leq E_{\max} \left[1 - \frac{e^{-z_0 t_1}}{z_0} \right]$$

$$\frac{\frac{1}{z_0} - \frac{e^{-z_0 t_1}}{\alpha+z_0}}{1 - \frac{e^{-z_0 t_1}}{z_0}} \leq E_{\max} \quad ; \quad E_{\max} \geq \frac{(\alpha+z_0) - z_0 e^{-z_0 t_1}}{(\alpha+z_0)(z_0 - e^{-z_0 t_1})}$$

Lower bound for E_{\max} in $[0, t_1]$

Problem 8.4, Goodwin et al. p 238

$$\text{Given } G_0(s) = \frac{5(s-1)}{(s+1)(s-5)}$$

This plant has to be controlled in a feedback loop with one-degree-of-freedom.

8.4.1. Determine time-domain constraints for the plant input, the plant output, and the control error in the loop. Assume exact inversion at $w=0$ and step-like reference and disturbances.

$$G_0(s) = \frac{B_0(s)}{A_0(s)} \quad C(s) = \frac{P(s)}{L(s)}$$

Uncancelled plant poles & zeros impose algebraic / interpolation constraints on the sensitivity functions.

NB: zero @ $s=1 \rightarrow B_0(1) = 0$
pole @ $s=5 \rightarrow A_0(5) = 0$
exact inversion @ $w=0 \rightarrow L(0) = 0$ in order to get $S_0(0) = 0 \Leftrightarrow T_0(0) = 1$

Interpolation constraints:

$$S_0(1) = \frac{A_0(1)L(1)}{A_0(1)L(1) + B_0(1)P(1)} = 1$$

$$S_0(5) = \frac{A_0(5)L(5)}{A_0(5)L(5) + B_0(5)P(5)} = 0$$

$$T_0(1) = \frac{B_0(1)P(1)}{A_0(1)L(1) + B_0(1)P(1)} = 0$$

$$T_0(s) = \frac{B_0(s) P(s)}{A_0(s) L(s) + B_0(s) P(s)} = 1$$

$$S_{i_0}(1) = \frac{B_0(1) L(1)}{A_0(1) L(1) + B_0(1) P(1)} = 0$$

$$S_{u_0}(s) = \frac{A_0(s) P(s)}{A_0(s) L(s) + B_0(s) P(s)} = 0$$

• Effect of unit step reference:

$$Y(s) = T_0(s) \cdot \frac{1}{s} \xrightarrow{s \rightarrow 1} \int_0^{\infty} y(t) e^{-t} dt = \lim_{s \rightarrow 1} T_0(s) \cdot \frac{1}{s} = 0 \cdot 1 = 0$$

$$\xrightarrow{s \rightarrow s} \int_0^{\infty} y(t) e^{-st} dt = \lim_{s \rightarrow s} T_0(s) \cdot \frac{1}{s} = 1 \cdot \frac{1}{s} = \frac{1}{s}$$

$$U(s) = S_{u_0}(s) \cdot \frac{1}{s} \xrightarrow{s \rightarrow s} \int_0^{\infty} u(t) e^{-st} dt = 0$$

$$E(s) = S_0(s) \cdot \frac{1}{s} \xrightarrow{s \rightarrow 1} \int_0^{\infty} e(t) e^{-t} dt = 1$$

$$\xrightarrow{s \rightarrow s} \int_0^{\infty} e(t) e^{-st} dt = 0$$

• Effect of unit step disturbance:

$$Y(s) = S_{i_0}(s) \cdot \frac{1}{s} \xrightarrow{s \rightarrow 1} \int_0^{\infty} y(t) e^{-t} dt = 0$$

$$U(s) = S_0(s) \cdot \frac{1}{s} \xrightarrow{s \rightarrow s} \int_0^{\infty} u(t) e^{-st} dt = 0$$

$$\xrightarrow{s \rightarrow 1} \int_0^{\infty} u(t) e^{-t} dt = 1$$

$$E(s) = -S_{i_0}(s) \cdot \frac{1}{s} \xrightarrow{s \rightarrow 1} \int_0^{\infty} e(t) e^{-t} dt = 0$$

• Effect of unit step disturbance:

$$Y(s) = S_0(s) \cdot \frac{1}{s} \xrightarrow{s=0} \int_0^{\infty} y(t) e^{-st} dt = 0$$
$$\xrightarrow{s=1} \int_0^{\infty} y(t) e^{-t} dt = 1$$

$$U(s) = -S_{u0}(s) \cdot \frac{1}{s} \xrightarrow{s=0} \int_0^{\infty} u(t) e^{-st} dt = 0$$

$$E(s) = -S_0(s) \cdot \frac{1}{s} \xrightarrow{s=0} \int_0^{\infty} e(t) e^{-st} dt = 0$$
$$\xrightarrow{s=1} \int_0^{\infty} e(t) e^{-t} dt = 1$$

8.4.2.

Why is the control of this nominal plant especially difficult?

→ contradicting requirements:

- the NMP zero sets an upper bound for the closed loop bandwidth since * indicates that if $y(t)$ settles much faster than e^{-t} , there will be a large undershoot.
- the unstable pole sets a lower bound for the closed loop bandwidth since * indicates that if $y(t)$ settles much slower than e^{-st} , there will be a large overshoot.