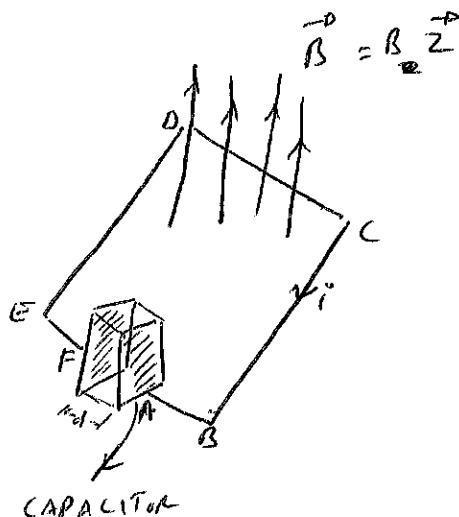
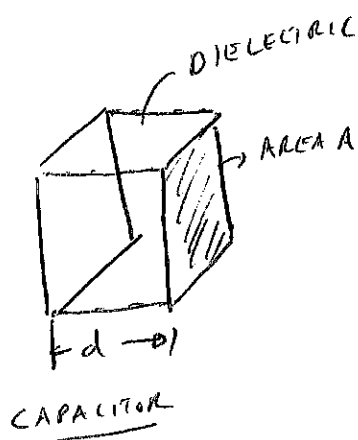


WORKED EXAMPLES: DISPLACEMENT CURRENT & FARADAY'S LAW



Q 2

THE MAGNETIC FLUX DENSITY LINKED WITH THE CONDUCTING LOOP 'ABCDEFA' IS GIVEN BY

$$\vec{B} = B_0 e^{\alpha t} \hat{z} \text{ T}$$

WHERE $\alpha = 2 \text{ s}^{-1}$, $B_0 = 500 \text{ T}$. THE AREA OF THE LOOP 'ABCDEFA' IS 20 cm^2 . THE LOOP IS IN THE XY PLANE. THE CAPACITANCE OF THE CAPACITOR IS 5 F . ASSUME THAT THE DIELECTRIC INSIDE THE CAPACITOR IS PERFECT (ZERO RESISTANCE). FIND (a) INDUCED EMF

- (b) ^{CONDUCTION} CURRENT DENSITY & ^{CONDUCTION} CURRENT IN THE CIRCUIT. ~~ASSUME THAT~~
- (c) ASSUME THAT THE CONDUCTORS ARE PERFECT (ZERO RESISTANCE)
- (d) DISPLACEMENT CURRENT ~~IN~~ THE DIELECTRIC.
- (e) CONDUCTION CURRENT & DISPLACEMENT IN THE CONDUCTOR & DISPLACEMENT CURRENT IN THE DIELECTRIC IF ~~IF~~

CONDUCTIVITY OF THE CONDUCTOR IS $5.5 \times 10^7 \text{ S/m}$. ASSUME

THAT THE LENGTH OF THE CONDUCTOR IS 3 m & CROSS-SECTIONAL AREA IS 0.5 mm^2 ; $\epsilon_r = \mu_r = 1$.

②

SOLUTION:

(a) THE MAGNETIC FLUX,

$$\begin{aligned}\Psi_m &= \int_S \vec{B} \cdot d\vec{s} = B_0 e^{\alpha t} \times (20 \times 10^{-4}) \text{ Wb} \\ &= e^{\alpha t} \text{ Wb} \quad (\because B_0 = 500 \text{ T}, \alpha = 2 \text{ s}^{-1})\end{aligned}$$

$$\begin{aligned}\text{EMF} = \mathcal{E} &= -\frac{d\Psi_m}{dt} = -2e^{\alpha t} \text{ V} \\ &= -2e^{2t} \text{ V}\end{aligned}$$

(b)

FOR A CAPACITOR,

$$q = C\mathcal{E}; \quad C = 5 \text{ F}$$

$$\begin{aligned}\therefore i &= \frac{dq}{dt} = C \frac{d\mathcal{E}}{dt} = C[-4e^{2t}] \text{ A} \\ &= -20e^{2t} \text{ A}\end{aligned}$$

NOTE THAT IN THIS CASE, THE CONDUCTOR IS PERFECT & HENCE, THERE IS NO VOLTAGE DROP ACROSS THE CONDUCTOR. THE EMF DEVELOPED DUE TO TIME-CHANGING MAGNETIC FIELD APPEARS AT THE CAPACITOR TERMINALS.

CONDUCTION CURRENT DENSITY,

$$\begin{aligned}i &= \frac{I}{A} \quad J = \frac{i}{S}, \\ J &= \frac{i}{S}\end{aligned}$$

WHERE S = CROSS-SECTIONAL AREA OF THE CONDUCTOR.

$$\textcircled{3} \quad J = \frac{-20 e^{2t}}{0.5 \times 10^{-3}} = -4 \times 10^7 e^{2t} \text{ A/m}^2$$

FOR A PERFECT CONDUCTOR, $\sigma = \infty$

$$J = \sigma E$$

SINCE $\sigma = \infty$, $E = 0$ & $D = 0$ IN THE CONDUCTOR.

THIS IMPLIES THAT THERE IS NO DISPLACEMENT CURRENT

IN THE CONDUCTOR ($\because J_d \neq \partial D / \partial t$).

\textcircled{c} IN THE CAPACITOR,

$$E = V/d$$

$$D = \epsilon E = \epsilon V/d$$

$$J_d = \frac{\partial D}{\partial t} = \frac{\epsilon}{d} \frac{dV}{dt}$$

$$\text{THE DISPLACEMENT CURRENT } i_d = \int \vec{J}_d \cdot d\vec{s} = \left(\frac{\epsilon}{d} \frac{dV}{dt} \right) \cdot A$$

$$= C \frac{dV}{dt} \quad (\because C = \frac{\epsilon A}{d})$$

= i = CONDUCTION CURRENT
IN THE CONDUCTORS

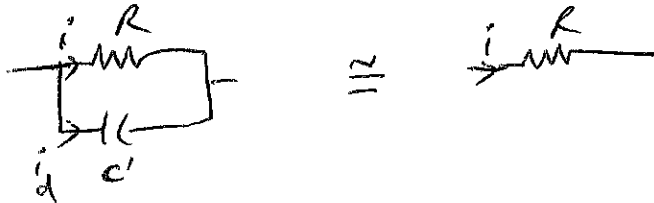
$$= -20 e^{2t} \text{ A.}$$

(d) WHEN THE CONDUCTOR IS NOT PERFECT, THERE EXISTS

A SMALL DISPLACEMENT CURRENT IN THE CONDUCTOR &

THE EQUIVALENT CIRCUIT OF THE CONDUCTOR MAY BE

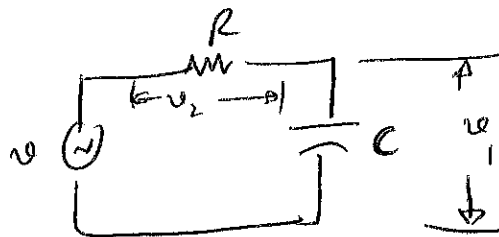
WRITTEN AS



HOWEVER, $i_d \ll i$. HENCE, THE CAPACITANCE OF THE CONDUCTOR

MAY BE IGNORED. NOW, THE EQUIVALENT CIRCUIT OF THE

LOOP 'ABCOEFA' MAY BE WRITTEN AS



FOR THE CASE OF (b) & (c), $\sigma = \infty \Rightarrow R = 0$. HENCE, THE

GENERATED emf, v APPEARS ACROSS C . NOW, WE NEED TO

TAKE INTO ACCOUNT THE VOLTAGE DROP IN CONDUCTORS.

$$R = \frac{l}{\sigma S}$$

l = LENGTH OF THE CONDUCTOR

σ = CONDUCTIVITY

S = CROSS-SECTIONAL AREA

$$= \frac{3}{5.5 \times 10^7 \times 0.5 \times 10^{-6}} \Omega$$

$$= 0.1091 \Omega$$

(5)

USING KVL, $v_1 + v_2 = v \rightarrow (1)$

$$v_2 = iR$$

CAPACITOR: $q = C v_1$

$$i = \frac{dq}{dt} \Rightarrow q = \int i dt$$

$$v_1 = \frac{1}{C} \int i dt$$

(1) BECOMES

$$\frac{1}{C} \int i dt + iR = v = -2 e^{2t}$$

DIFFERENTIATING, WE GET

$$\frac{i}{R} + R \frac{di}{dt} = -4 e^{2t}$$

$$\frac{i}{\tau} + \frac{di}{dt} = \frac{-4}{R} e^{2t}$$

$$= -36.66 e^{2t} \rightarrow (2)$$

WHERE $\tau = RC = 0.1091 \times 5 = 0.5455 \text{ s}$

LET $i = x e^{-t/\tau}$

$$\frac{di}{dt} = \frac{dx}{dt} e^{-t/\tau} - \frac{x}{\tau} e^{-t/\tau} \rightarrow (3)$$

$$\frac{i}{\tau} = \frac{x}{\tau} e^{-t/\tau} \rightarrow (4)$$

USING (3) & (4) in (2), WE FIND

6

$$\frac{dx}{dt} = -36.66 e^{2t} \times e^{t/\tau}$$

$$x = \frac{-36.66 e^{(2+1/\tau)t}}{(2+1/\tau)}$$

$$i = x e^{-t/\tau} = \frac{-36.66}{2+1/\tau} e^{2t}$$

$$= -9.5639 e^{2t} \text{ A}$$

$$J = \frac{i}{S} = \frac{-9.5639 e^{2t}}{0.5 \times 10^{-3} \text{ m}^2} \text{ A/m}^2$$

$$= -1.9128 \times 10^7 e^{2t} \text{ A/m}^2$$

$$J = \sigma E$$

$$E = \frac{J}{\sigma} = \frac{-1.9128 \times 10^7 e^{2t}}{5.5 \times 10^7} \text{ V/m}$$

$$= -0.3478 e^{2t} \text{ V/m}$$

$$D = \epsilon_0 \epsilon_r E = \epsilon_0 E \quad (\because \epsilon_r = 1)$$

$$\epsilon_0 = 8.854 \times 10^{-12} \text{ F/m}$$

$$J_d = \frac{\partial D}{\partial t} = \epsilon_0 \frac{\partial E}{\partial t} = 8.854 \times 10^{-12} \times 0.3478 \times 2 \times e^{2t} \text{ A/m}^2$$

$$= 6.146 \times 10^{-12} \text{ A/m}^2$$

(7)

$$i_d = J_d S = 6.146 \times 10^{-12} \times 0.5 \times (10^{-3})^2 \text{ A}$$
$$= 3.073 \times 10^{-18} \text{ A}$$

NOTE $i_d \ll i$ IN THE CONDUCTOR

DISPLACEMENT CURRENT IN THE CAPACITOR?

$$E = \frac{v_1}{d}$$

v_1 = VOLTAGE ACROSS THE CAPACITOR

$$D = \epsilon E = \epsilon \frac{v_1}{d}$$

$$J_d = \frac{\partial D}{\partial t} = \frac{\epsilon}{d} \frac{dv_1}{dt}$$

$$i_d = J_d A = \epsilon \frac{dv_1}{dt}$$

$$v_1 = v - v_2 = v - iR$$
$$= -2e^{2t} + 9.5639e^{2t} \times 0.109 \text{ V}$$
$$= -0.9567e^{2t} \text{ V}$$

$$i_d = 5 \times (-0.9567) \times 2e^{2t} \text{ A}$$
$$= -9.567e^{2t} \text{ A}$$

Note that ~~the~~ conduction current in the conductor is the same as the displacement current in capacitor (displacement current in the conductor may be ignored)