

POWER TRANSMISSION :

(1)

CIRCUITS :

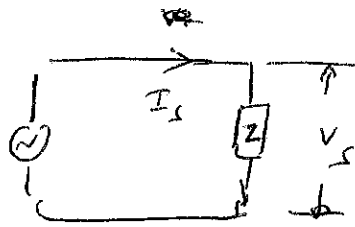


FIG. 1

THE MEAN POWER DISSIPATED IN AN IMPEDANCE, Z IS

$$\langle P \rangle = \frac{1}{2} \operatorname{Re} \{ V_s I_s^* \} \quad \rightarrow (1)$$

WHERE V_s IS THE VOLTAGE ACROSS Z & I_s IS THE CURRENT THROUGH Z , IN THE PHASOR NOTATION. ~~IF YOU ARE NOT~~

FAMILIAR WITH (1), USE

$$v = \operatorname{Re} \{ V_s e^{j\omega t} \} = V_p \cos(\omega t + \theta_v)$$

$$i = \operatorname{Re} \{ I_s e^{j\omega t} \} = I_p \cos(\omega t + \theta_i)$$

$$P = v i$$

$$= V_p I_p \cos(\omega t + \theta_v) \cos(\omega t + \theta_i) \quad \text{PERIOD}$$

$$\langle P \rangle = \frac{1}{T} \int_0^T V_p I_p \cos(\omega t + \theta_v) \cos(\omega t + \theta_i) dt$$

$$= \frac{1}{2} \operatorname{Re} \{ V_s I_s^* \} \quad \rightarrow \text{PROVE ~~THE~~}$$

(2)

TRANSMISSION LINES

WE USE EQ. (1) TO EXPRESS POWER AT ANY POINT IN THE TRANSMISSION LINE.

$$\langle P(z) \rangle = \frac{1}{2} \operatorname{Re} \{ V_S(z) I_S^*(z) \}$$

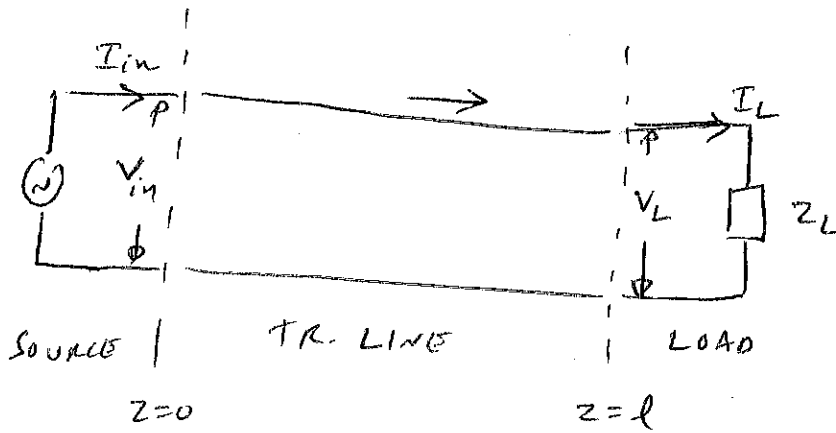


FIG. 2

AT THE SOURCE, $z=0$, $\langle P(z) \rangle = P_{in}$

$$V_S(0) = V_{in}$$

$$I_S(0) = I_{in}$$

$$\therefore P_{in} = \frac{1}{2} \operatorname{Re} \{ V_{in} I_{in}^* \}$$

AT THE LOAD, $z=l$, $\langle P(z=l) \rangle = P_L$

$$V_S(l) = V_L$$

$$I_S(l) = I_L$$

$$\therefore P_L = \frac{1}{2} \operatorname{Re} \{ V_L I_L^* \}$$

③

LET US ASSUME THAT THE CHARACTERISTIC IMPEDANCE, Z_0
 IS EQUAL TO Z_L SO THAT THERE IS NO REFLECTION.

IN THIS CASE, THERE IS ONLY FORWARD PROPAGATING WAVE

$$V_s(z) = V_0^+ e^{-\gamma z} = V_0^+ e^{-(\alpha + j\beta)z}$$

$$I_s(z) = I_0^+ e^{-\gamma z} = \frac{V_0^+}{Z_0} e^{-\gamma z}$$

$$\gamma = (\alpha + j\beta)$$

$$\text{AT } z=0, V_s(0) = V_{in} = V_0^+ e^0 = V_0^+$$

$$I_s(0) = I_{in} = I_0^+ e^0 = \frac{V_0^+}{Z_0}$$

$$\langle P(0) \rangle = P_{in} = \frac{1}{2} \operatorname{Re} \left\{ \frac{V_0^+ (V_0^+)^*}{Z_0^*} \right\}$$

$$\text{LET } Z_0 = |Z_0| e^{j\theta_0}$$

$$\therefore P_{in} = \frac{1}{2} \operatorname{Re} \left\{ \frac{|V_0^+|^2}{|Z_0|} e^{+j\theta_0} \right\}$$

$$= \frac{|V_0^+|^2}{2|Z_0|} \cos \theta_0 \quad \rightarrow \textcircled{2}$$

$$\text{AT ANY } z, \langle P(z) \rangle = \frac{1}{2} \operatorname{Re} \left\{ V_s(z) I_s^*(z) \right\}$$

$$= \frac{1}{2} \operatorname{Re} \left\{ V_0^+ \frac{(V_0^+)^*}{Z_0^*} e^{-2\alpha z} \right\}$$

$$= P_{in} \cdot e^{-2\alpha z} \quad \rightarrow \textcircled{3}$$

POWER LOSS IN dB ~~OR~~ UNITS ⁽⁴⁾ IS EXPRESSED AS

$$\text{POWER LOSS (dB)} = -10 \log_{10} \left[\frac{P(z)}{P(0)} \right] \rightarrow (4)$$

NOTE: $P(z) < P(0)$ & HENCE, $\log_{10} [P(z)/P(0)]$ IS NEGATIVE.

TYPICALLY, WE LIKE TO EXPRESS THE LOSS OF POWER DUE TO PROPAGATION FROM 0 TO Z AS POSITIVE. SO, -VE SIGN IS ~~BE~~ INTRODUCED IN (4).

USING (3) IN (4), WE FIND

$$\text{POWER LOSS (dB)} = -10 \log_{10} \left(\frac{P_0 e^{-\alpha z}}{P_0} \right)$$

$$= -10 \frac{\log_e (e^{-\alpha z})}{\log_e 10} \quad - 2.3026 \alpha z$$

$$\boxed{\text{POWER LOSS (dB)} = 8.69 \alpha z} \rightarrow (5)$$

LOSS RATING IS ~~EXP~~ THE POWER LOSS IN dB PER UNIT LENGTH, I.E.

$$\boxed{\text{LOSS RATING (dB/m)} = \frac{\text{POWER LOSS (dB)}}{z} = 8.69 \alpha} \rightarrow (6)$$

NOTE: α SHOULD IN THE UNIT OF NP/M OR M⁻¹.

$$\langle P(z) \rangle = \frac{1}{2} \operatorname{Re} \left\{ V_s(z) I_s^*(z) \right\} \quad (5)$$

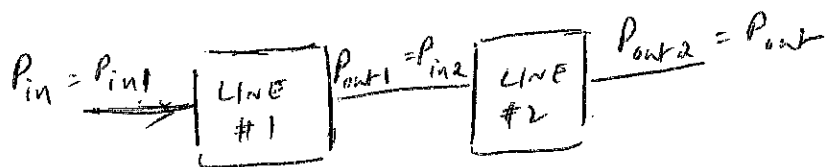
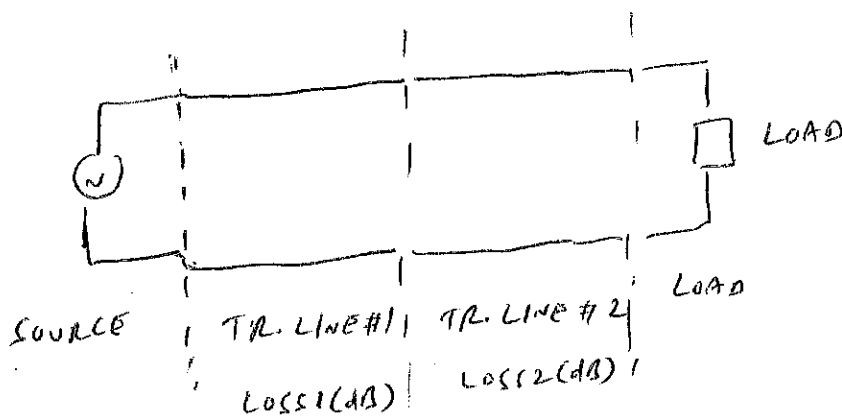
$$= \frac{1}{2} \operatorname{Re} \left\{ V_s(z) \frac{V_s^*(z)}{Z_0^*} \right\} = \frac{|V_s(z)|^2}{2} \operatorname{Re} \left\{ \frac{1}{Z_0^*} \right\}$$

$$P_{in} = \frac{1}{2} \operatorname{Re} \left\{ V_s(\omega) \frac{V_s^*(\omega)}{Z_0^*} \right\} = \frac{|V_s(\omega)|^2}{2} \operatorname{Re} \left\{ \frac{1}{Z_0^*} \right\}$$

∴ (4) CAN BE WRITTEN AS

$$\text{POWER LOSS (dB)} = -10 \log_{10} \frac{|V_s(z)|^2}{|V_s(\omega)|^2}$$

$$\text{POWER LOSS (dB)} = -20 \log_{10} \frac{|V_s(z)|}{|V_s(\omega)|}$$



$$\text{LOSS 1 (dB)} = -10 \log_{10} \left(\frac{P_{out1}}{P_{in1}} \right)$$

$$\text{LOSS 2 (dB)} = -10 \log_{10} \left(\frac{P_{out2}}{P_{in2}} \right)$$

$$\begin{aligned}
 \text{Total loss (dB)} &= -10 \log_{10} \left(\frac{P_{out}}{P_{in}} \right) \quad \text{⑥} \\
 &= -10 \log_{10} \left(\frac{P_{out2}}{P_{in2}} \frac{P_{in2}}{P_{in1}} \right) \\
 &= -10 \left[\log_{10} \left(\frac{P_{out2}}{P_{in2}} \right) + \log_{10} \left(\frac{P_{in2}}{P_{in1}} \right) \right]
 \end{aligned}$$

$$\boxed{\text{TOTAL LOSS (dB)} = \text{LOSS1 (dB)} + \text{LOSS2 (dB)}}$$

THE ADVANTAGE OF DECIBEL UNIT IS THAT LOSSES/GAINS IN THE SYSTEM CAN BE ADDED/SUBTRACTED. IN CONTRAST, IF WE USE $e^{-\alpha z}$ TO MODEL LOSS, MULTIPLICATIONS WILL BE REQUIRED.

EXAMPLE: TR. LINE#1 SHOWN IN FIG. 3 HAS AN ATTENUATION COEFFICIENT OF 0.01 NP/m & ~~LINE #2~~ IT IS 20m long. LINE #2 IS RATED AT 0.1 dB/m & IS 15m long. THE JOINT IS NOT WELL DONE & THE CONNECTION LOSS IS 2 dB. FIND THE TOTAL LOSS.

$$\langle P(z) \rangle = P_{in} e^{-2\alpha z}$$

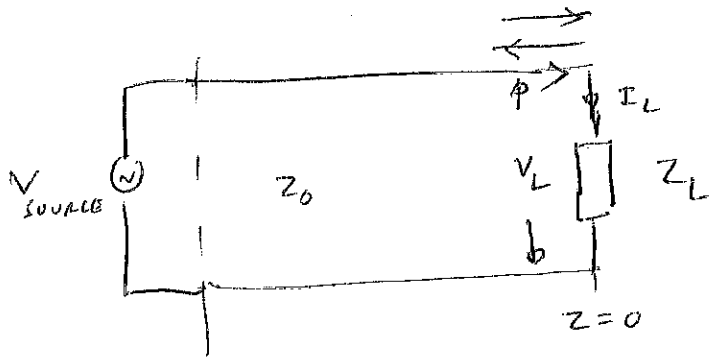
$$\begin{aligned}
 \text{FROM (5), POWER LOSS1 (dB)} &= 8.69 \alpha z \\
 &= 8.69 \times 0.01 \times 20 \text{ dB} \\
 &= 1.738 \text{ dB}
 \end{aligned}$$

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$$\begin{aligned} \text{POWER LOSS 2 (dB)} &= 0.1 \frac{\text{dB}}{\text{m}} \times 15 \text{ m} \\ &= 1.5 \text{ dB} \end{aligned}$$

$$\begin{aligned} \text{TOTAL LOSS (dB)} &= \text{loss 1 (dB)} + \text{loss 2 (dB)} + \text{connection loss (dB)} \\ &= 1.738 + 1.5 + 2 \text{ dB} \\ &= 5.238 \text{ dB} \end{aligned}$$

POWER REFLECTION



THE REFLECTION COEFFICIENT IS DEFINED AS (SEE

NOTES ON WAVE REFLECTION)

$$\Gamma = \frac{\text{AMPLITUDE OF THE } \overset{\text{BACKWARD}}{\cancel{\text{FORWARD}}} \text{ WAVE AT LOAD}}{\text{AMPLITUDE OF THE FORWARD WAVE AT LOAD}}$$

$$= \frac{V_0^-}{V_0^+}$$

THE AVERAGE POWER OF THE \oplus WAVE \rightarrow FORWARD AT LOAD

$$\begin{aligned}
 = \langle P^+(z) \rangle &= \frac{1}{2} \operatorname{Re} \{ V_0^+ (I_0^+)^* \} \\
 &= \frac{1}{2} \operatorname{Re} \left\{ V_0^+ \left(\frac{V_0^+}{Z_0} \right)^* \right\} \\
 &= \frac{1}{2} |V_0^+|^2 \operatorname{Re} \left\{ \frac{1}{Z_0^*} \right\}
 \end{aligned}$$

THE AVERAGE POWER OF THE \ominus WAVE \rightarrow REFLECTED @ LOAD

$$= \langle P^-(z) \rangle = \frac{1}{2} \operatorname{Re} \{ V_0^- (I_0^-)^* \}$$

$$\frac{V_0^-}{I_0^-} = -Z_0$$

$$\therefore \langle P^-(z) \rangle = -\frac{1}{2} |V_0^-|^2 \operatorname{Re} \left\{ \frac{1}{Z_0^*} \right\}$$

-VE SIGN INDICATES THE POWER IS DIRECTED IN
 $-z$ DIRECTION. SINCE WE ARE INTERESTED ONLY IN THE
 MAGNITUDE OF POWER, WE WILL OMIT THE SIGN.

THE FRACTION OF INCIDENT POWER THAT IS REFLECTED IS

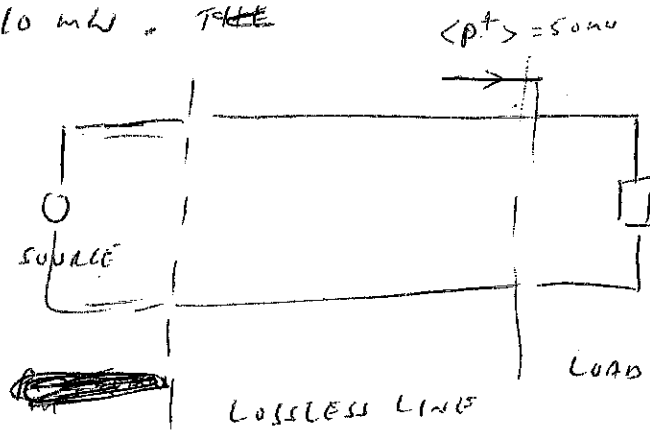
$$\frac{|\langle P^-(z) \rangle|}{|\langle P^+(z) \rangle|} = \frac{\frac{1}{2} |V_0^-|^2 \operatorname{Re} \left\{ \frac{1}{Z_0^*} \right\}}{\frac{1}{2} |V_0^+|^2 \operatorname{Re} \left\{ \frac{1}{Z_0^*} \right\}} = \frac{|V_0^-|^2}{|V_0^+|^2} = |\Gamma|^2$$

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THE FRACTION OF THE ~~REF~~ INCIDENT POWER THAT IS TRANSMITTED ~~OR~~ INTO THE LOAD (OR DISSIPATED BY IT) IS

$$\frac{\langle P_{*}(z) \rangle}{\langle P^{+}(z) \rangle} = \frac{|\langle P^{+} \rangle| - |\langle P^{-} \rangle|}{|\langle P^{+} \rangle|} = 1 - |\Gamma|^2$$

FOR EXAMPLE, ^{SUPPOSE} ~~IF~~ THE INCIDENT POWER ON A ~~LOSSLESS~~ LOSSLESS TRANSMISSION LINE IS 50 MW & THE REFLECTED POWER IS 10 MW, ~~THE~~



THE FRACTION OF THE INCIDENT POWER THAT IS REFLECTED IS $10/50 = 0.2$.

$$\therefore |\Gamma|^2 = 0.2$$

THE POWER DISSIPATED ~~BY~~ ^{BY} THE LOAD IS $50 - 10 = 40 \text{ MW}$.

THE FRACTION OF THE INCIDENT POWER THAT IS TRANSMITTED (OR DISSIPATED BY THE LOAD) IS

$$1 - |\Gamma|^2 = 0.8$$