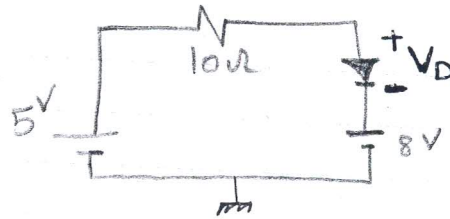


5-8

a)



6 → Practical model

7 → ideal model

8 → complete model

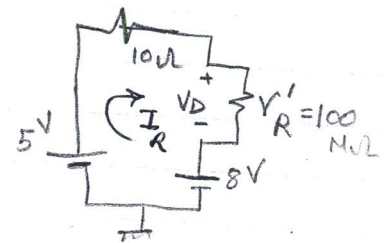
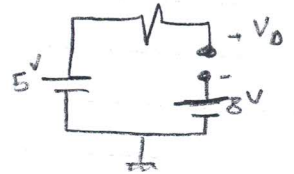
5 The diode is reverse-biased

6, 7  $V_D = V_R = 5 - 8 = -3V$

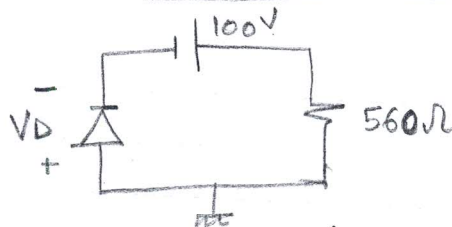
8  $V_D = I_R r'_R$

$$I_R = \frac{5 - 8}{10 + 100 \times 10^6} = \frac{-3}{10 + 100 \times 10^6} = -2.999 \times 10^{-8}$$

$V_D = -2.999 \text{ volt}$   
 $\approx -3V$

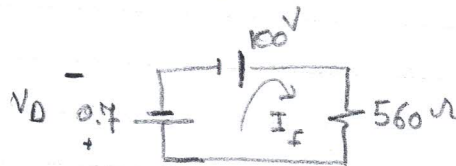


b)



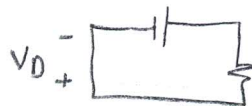
5 Forward biased

6



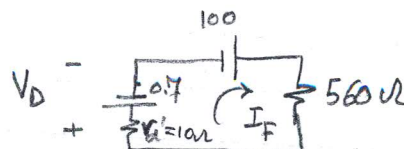
$V_D = V_F = 0.7V$ ,  $I_F = \frac{100 - 0.7}{560} \text{ A}$

7



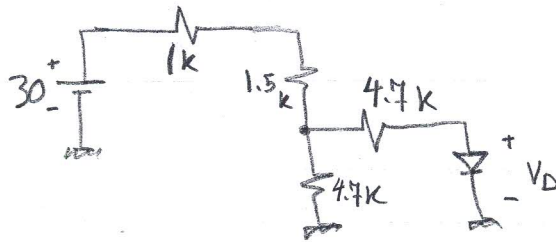
$V_D = V_F = 0V$ ,  $I_F = \frac{100}{560} \text{ A}$

8



$V_D = 0.7 + I_F r'_d$ ,  $I_F = \frac{100 - 0.7}{10 + 560} = 174.21 \text{ mA}$   
 $V_D = 2.442V$

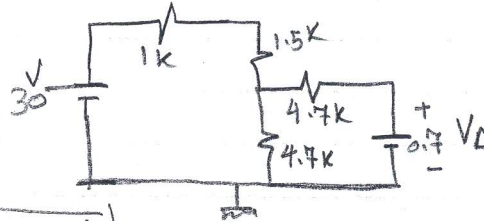
c)



(2)

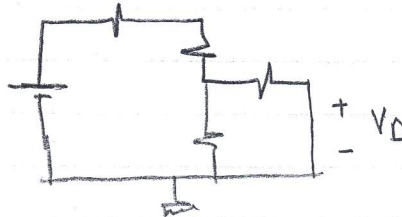
5 Forward - biased

6



$$V_D = V_F = 0.7V$$

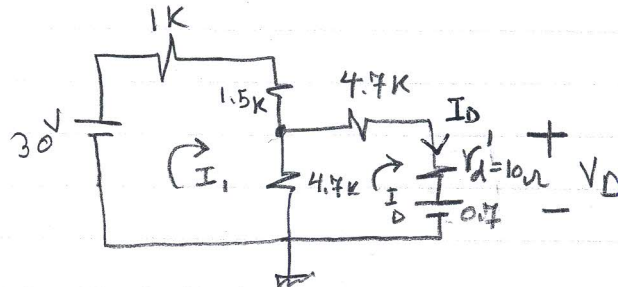
7



$$V_D = 0V$$

8

$$V_D = 0.7 + I_D r_d'$$



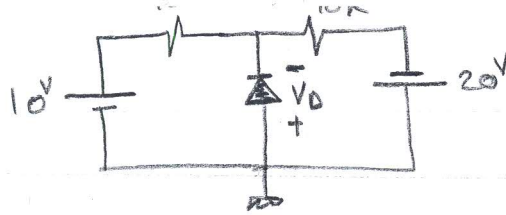
$$(1+1.5)k I_1 + 4.7k(I_1 - I_D) - 30 = 0 \quad \text{or} \quad 7.2k I_1 - 4.7k I_D = 30$$

$$(4.7k + 10)I_D + 0.7 + 4.7k(I_D - I_1) = 0 \quad \text{or} \quad -4.7k I_1 + 9410 I_D = -0.7$$

$$I_D = 2.97453 \text{ mA}$$

$$V_D = 0.7298 \text{ V}$$

d)

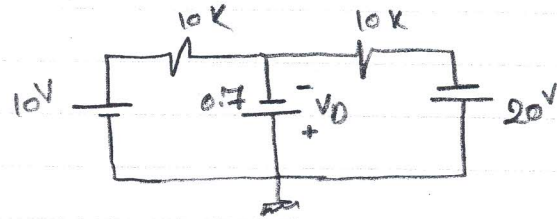


(3

5 Forward biased

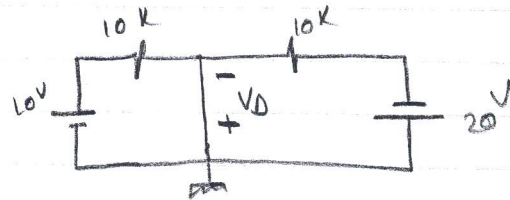
6

$$V_D = V_F = 0.7V$$



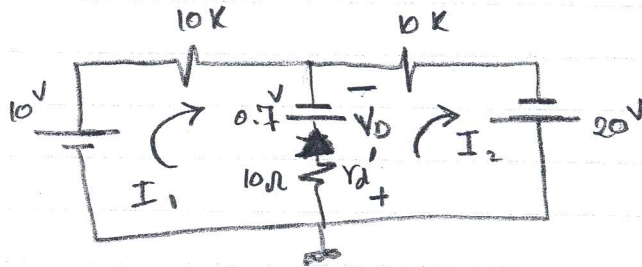
7

$$V_D = 0V$$



8

$$V_D = 0.7 + (I_2 - I_1) r_d'$$



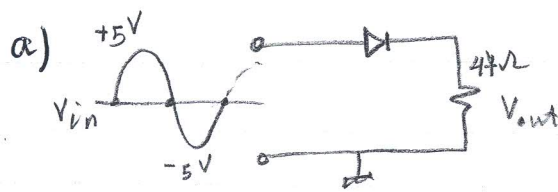
$$10k I_1 - 0.7 + (I_1 - I_2) 10 - 10V = 0 \quad \text{or} \quad 1.01k I_1 - 0.01k I_2 = 10.7$$

$$10k I_2 - 20 + (I_2 - I_1) 10 + 0.7 = 0 \quad \text{or} \quad -0.01k I_1 + 1.01k I_2 = 19.3$$

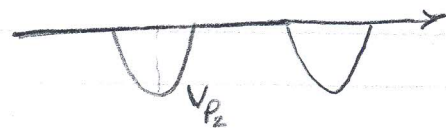
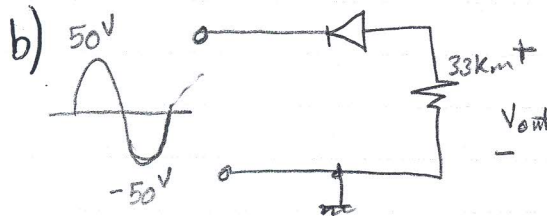
$$\therefore I_1 = 10.784 \text{ mA}, \quad I_2 = 19.2157 \text{ mA}$$

$$\therefore V_D = 0.7843 \text{ V}$$

9



$V_{P1} = 5V$ , in case of ideal model  
 $V_{P1} = 5 - 0.7 = 4.3V$ , in case of practical model



$V_{P2} = -50V$ , in case of ideal model of diode

$V_{P2} = -49.3V$ , " " " " Practiced model " "  
 $= 0.7 - 50$

10

a)  $PIV = +V_{P1}(in) = +5V$

b)  $PIV = +V_{P2}(in) = +50V$

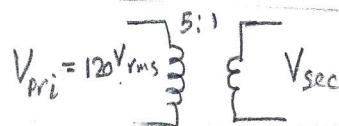
11

$$V_{Avg} = \frac{V_P}{\pi} = \frac{200}{\pi} \approx 63.662 V$$

as

$$V_{Avg} = \frac{1}{2\pi} \int_0^{2\pi} V_P \sin t dt = \frac{V_P}{2\pi} \int_0^{\pi} \sin t dt = \frac{V_P}{2\pi} [-\cos t]_0^{\pi} = \frac{V_P}{\pi}$$

13



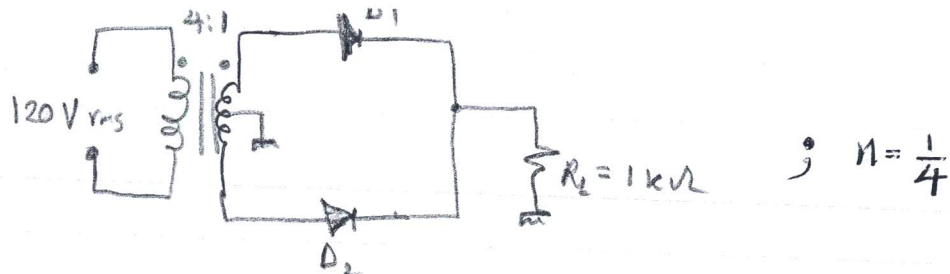
turns ratio "n"  $= \frac{N_{sec}}{N_{pri}} = \frac{1}{5} = \frac{V_{sec}}{V_{pri}}$

$\therefore V_{sec} = \frac{1}{5} V_{pri}$

$V_{sec} = 24 V_{rms}$



16



(5)

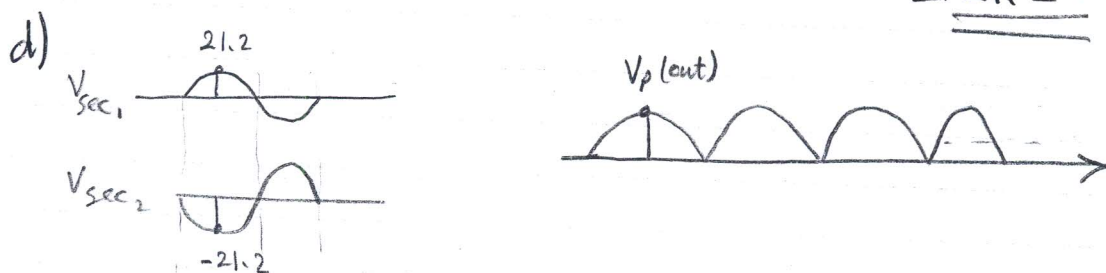
a) The circuit is a center-tapped full-wave rectifier

b)  $V_{rms}(sec) = n V_{rms}(pri) = \frac{1}{4} \times 120 = 30 \text{ V rms}$

$$\therefore V_p = \sqrt{2} V_{rms}$$

$$\therefore V_p(sec) = \sqrt{2} \times 30 = 42.43 \text{ V} \approx \underline{\underline{42.4 \text{ V}}}$$

c) Peak voltage across each half =  $\frac{V_p}{2} = 21.213 \text{ V}$   
 $\approx \underline{\underline{21.2 \text{ V}}}$

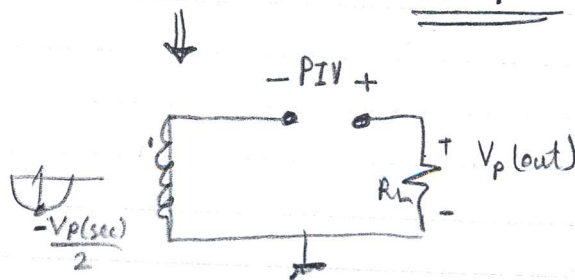


$$V_{RL}(P) = V_{p(out)} = 21.2 - 0.7 = \underline{\underline{20.5 \text{ V}}}$$

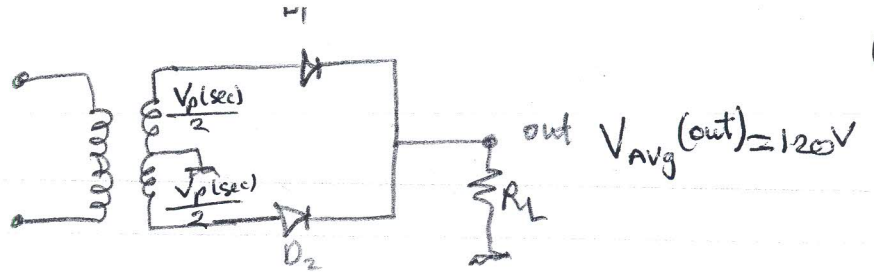
e)

$$I_P^{(D)} = \frac{\frac{V_p(sec)}{2} - 0.7}{R_L} = \frac{21.2 - 0.7}{1K} = \underline{\underline{20.5 \text{ mA}}}$$

f)  $PIV = V_{p(out)} - \left( \frac{-V_{p(sec)}}{2} \right)$  ; in inverse-biased case  
 $= 20.5 - (-21.2) = \underline{\underline{41.7 \text{ V}}}$



17



for a full-wave rectifier

$$V_{\text{avg}} = \frac{2 V_p}{\pi}$$

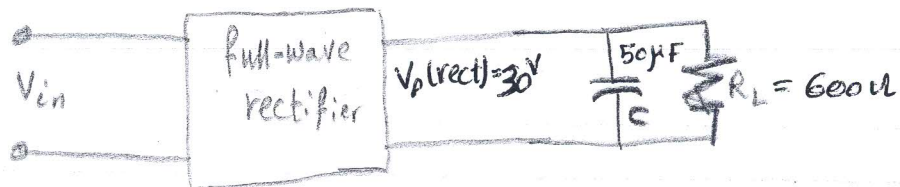
$$\therefore V_p(\text{out}) = \frac{\pi}{2} V_{\text{avg}}(\text{out}) = \frac{\pi}{2} * 120 = 60\pi \text{ V}$$

$$\therefore V_p(\text{out}) = \frac{V_p(\text{sec})}{2} - 0.7$$

$$\therefore \frac{V_p(\text{sec})}{2} = V_p(\text{out}) + 0.7$$

$$\therefore \frac{V_p(\text{sec})}{2} = 60\pi + 0.7 \approx 188.496 + 0.7$$
$$\approx \boxed{189.2 \text{ V}}$$

23



Let frequency of input signal = 60 Hz

$$\therefore f(\text{rect}) = 120 \text{ Hz}$$

$$\therefore V_r(\text{pp}) = \frac{V_p(\text{rect})}{f C R_L} = \frac{30}{(120)(50 \times 10^{-6})(600)}$$

$$\therefore V_r(\text{pp}) = 8.33 \text{ V} \rightarrow 8 \frac{1}{3}$$

$$V_{DC} = \left(1 - \frac{1}{2fR_L C}\right) V_p(\text{rect})$$

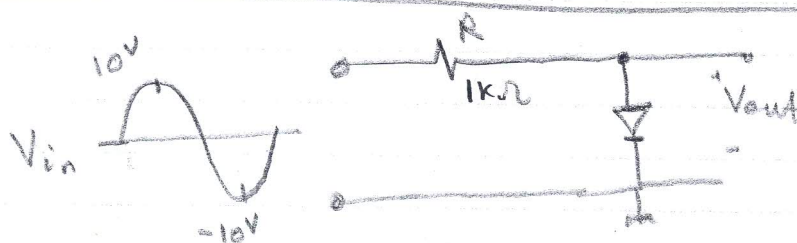
$$= \left[1 - \frac{1}{2 \times 120 \times 600 \times 50 \times 10^{-6}}\right] (30)$$

$$\therefore V_{DC} = 25.83 \text{ V}$$

24

$$\therefore \text{ripple factor } (r) = \frac{V_r(\text{pp})}{V_{DC}} = 32.25 \%$$

31



→ +ve clipper

when

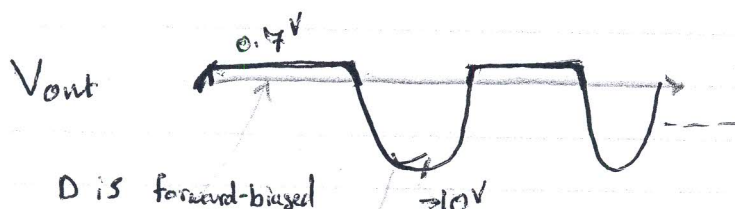
$$V_D = V_{in} > 0.7$$

D is forward-biased

$$\therefore V_{out} = V_F = 0.7 \text{ V}$$

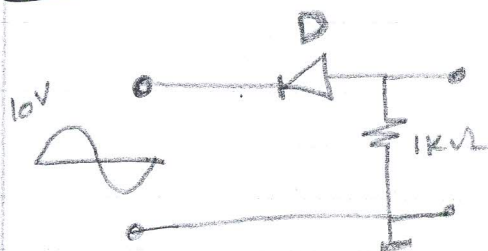
D is reverse-biased ⇒ open circuit

$$\therefore V_{out} = V_{in}$$



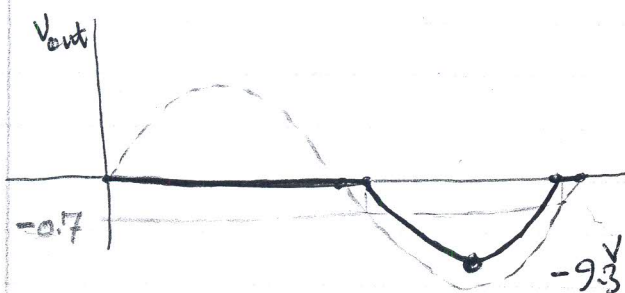
33

a)

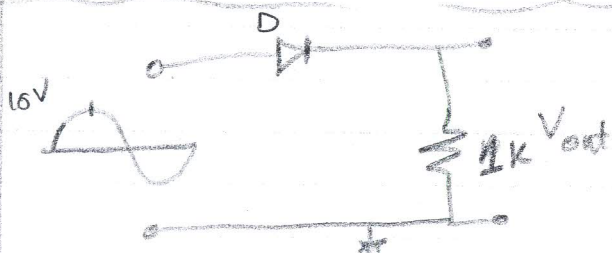


D is forward biased if:  $V_{in} \leq -0.7$

$$\rightarrow V_{out} = 0.7 + V_{in}$$

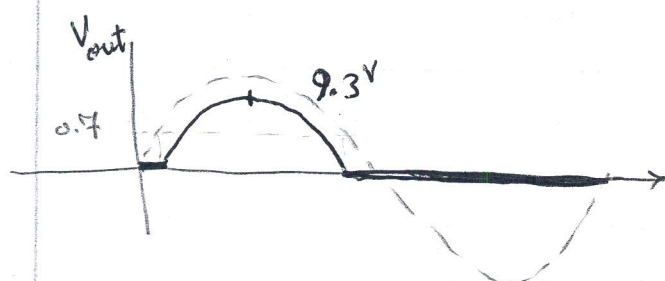


b)

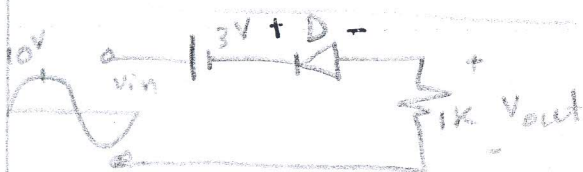


D is F.B. if:  $V_{in} \geq 0.7$

$$\rightarrow V_{out} = V_{in} - 0.7$$



c)

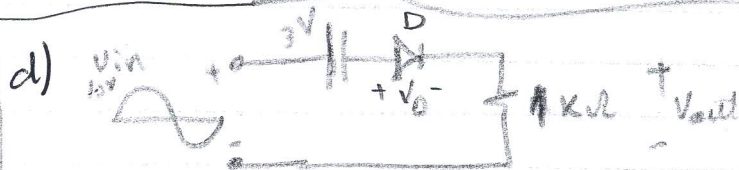
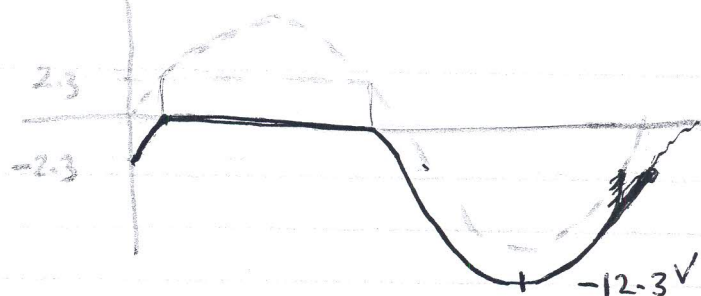


D is F.B.:  $V_D = -3 + V_{in} \leq -0.7$

$$\text{i.e. } V_{in} \leq -2.3V$$

$$\rightarrow V_{out} = 0.7 - 3 + V_{in} = -2.3 + V_{in}$$

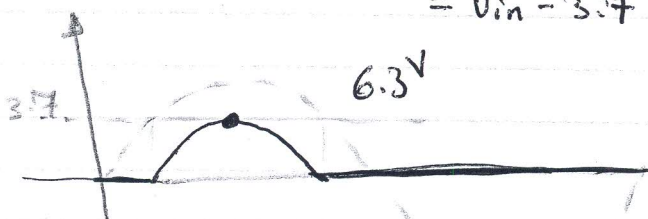
Vout



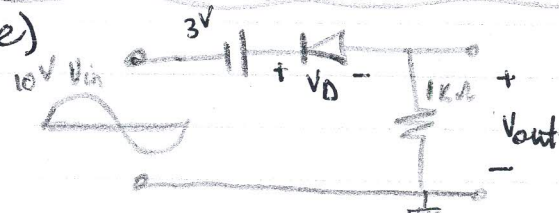
D is F.B.:  $V_D = -3 + V_{in} \geq 0.7$

$$V_{in} \geq 3.7V$$

$$\rightarrow V_{out} = -0.7 - 3 + V_{in} = V_{in} - 3.7$$



e)

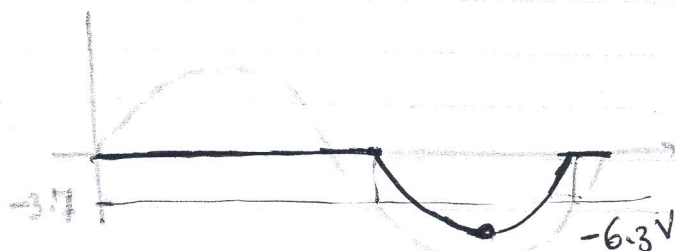


Dis F.B:

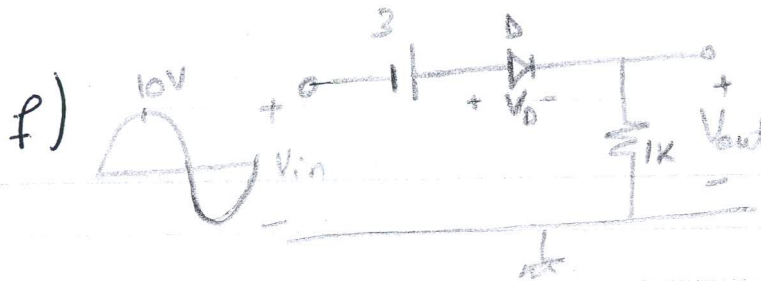
$$V_D = 3 + V_{in} \leq -0.7$$

$$\text{i.e. } V_{in} \leq -3.7$$

$$\rightarrow V_{out} = 0.7 + 3 + V_{in} = 3.7 + V_{in}$$

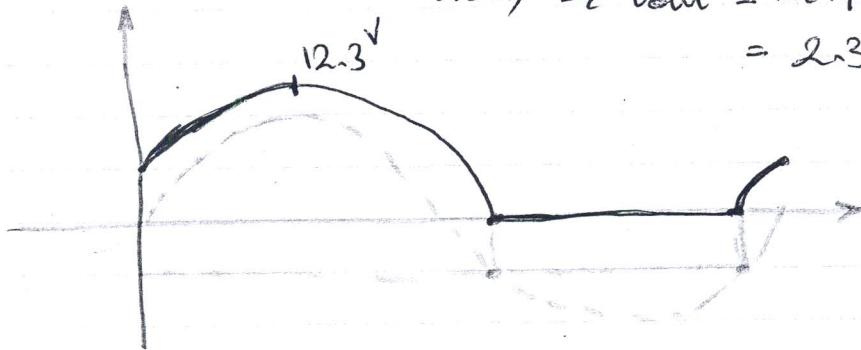






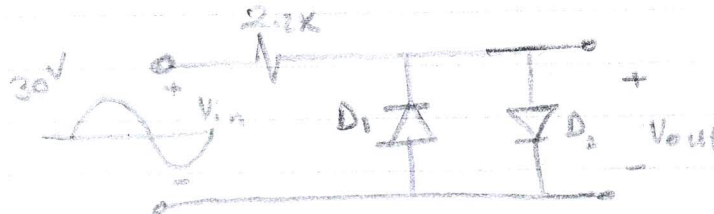
D is forward-biased :  $V_D = 3 + v_{in} \geq 0.7$   
 $v_{in} \geq -2.3 \text{ V}$

then,  $\Rightarrow v_{out} = -0.7 + 3 + v_{in}$   
 $= 2.3 + v_{in}$



35

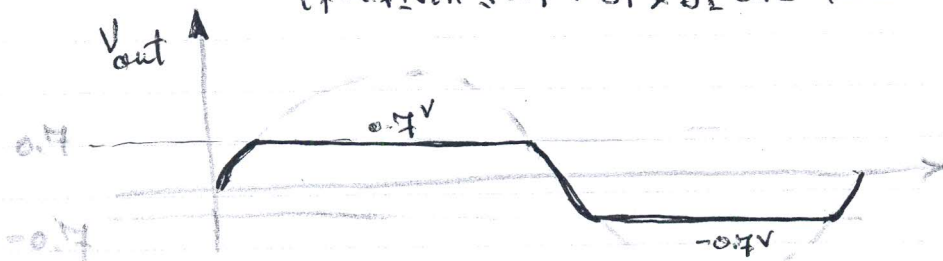
a)



$D_1$  is F.B. :  $v_{in} \leq -0.7 \Rightarrow v_{out} = -0.7 \text{ V}$

$D_2$  is F.B. :  $v_{in} \geq 0.7 \Rightarrow v_{out} = 0.7 \text{ V}$

if  $-0.7 \leq v_{in} \leq 0.7 \Rightarrow D_1 \& D_2$  are R.B.  $\Rightarrow v_{out} = v_{in}$



b)

$v_{out}$

$\downarrow D_1: \text{F.B.}$

0.7

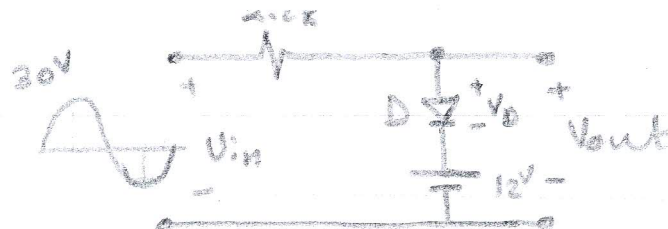
-0.7V

$\uparrow D_2: \text{F.B.}$

38

(10)

a)

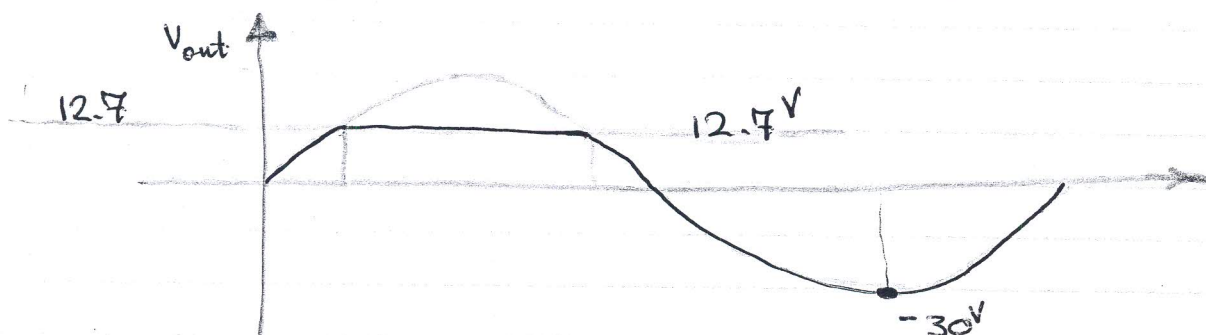


D is forward-biased:  $V_D = V_{in} - 12 \geq 0.7$

$$V_{in} \geq 12.7$$

$$\rightarrow V_{out} = 0.7 + 12 = 12.7V$$

if  $V_{in} < 12.7V$ , D is R.B.  $\Rightarrow V_{out} = V_{in}$



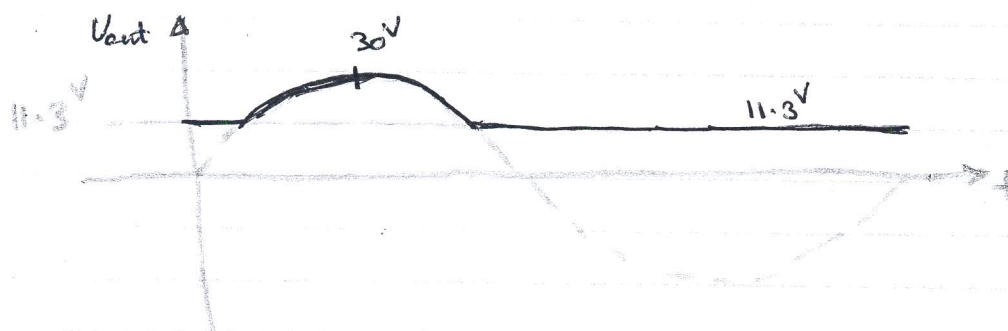
b)

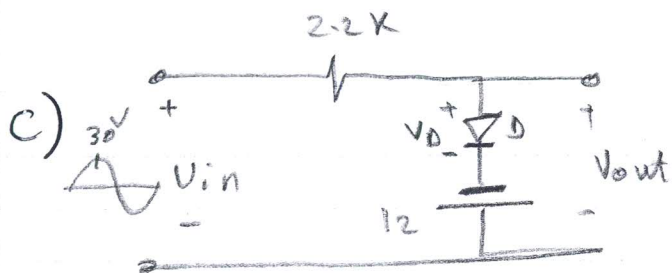


D is F.B.:  $V_D = V_{in} - 12 \leq -0.7 \rightarrow V_{in} \leq 11.3$

$$\rightarrow V_{out} = -0.7 + 12 = 11.3V$$

if  $V_{in} > 11.3V$ ; D is R-B;  $\rightarrow V_{out} = V_{in}$





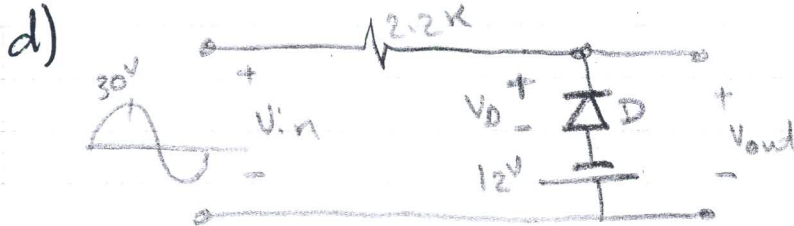
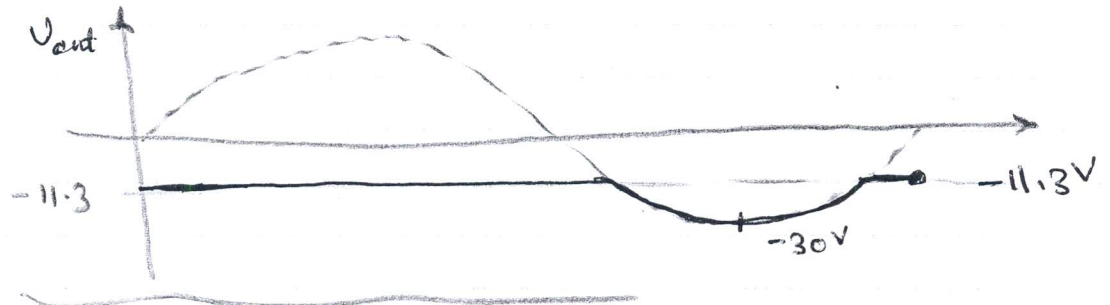
D is F-B :

$$V_D = V_{in} + 12 \geq 0.7$$

$$\Rightarrow V_{in} \geq -11.3V$$

$$\rightarrow V_{out} = 0.7 - 12 = -11.3V$$

@  $V_{in} < -11.3 \rightarrow$  D is R-B :  $V_{out} = V_{in}$



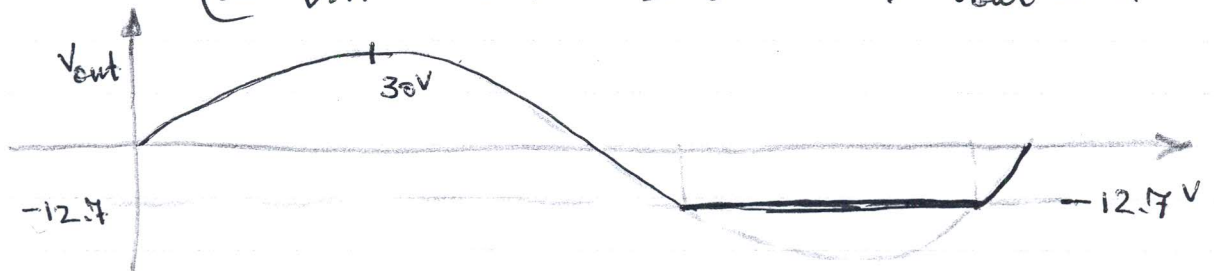
D is F-B!

$$V_D = V_{in} + 12 \leq -0.7$$

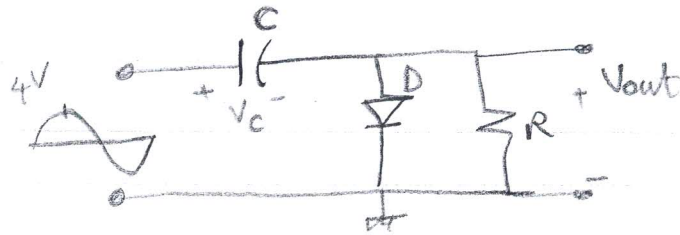
$$V_{in} \leq -12.7V$$

$$\rightarrow V_{out} = -12.7V$$

@  $V_{in} > -12.7V$  , D is R-B  $\rightarrow V_{out} = V_{in}$



(39) a)



after charging:  $V_c = V_p(\text{in}) - 0.7$

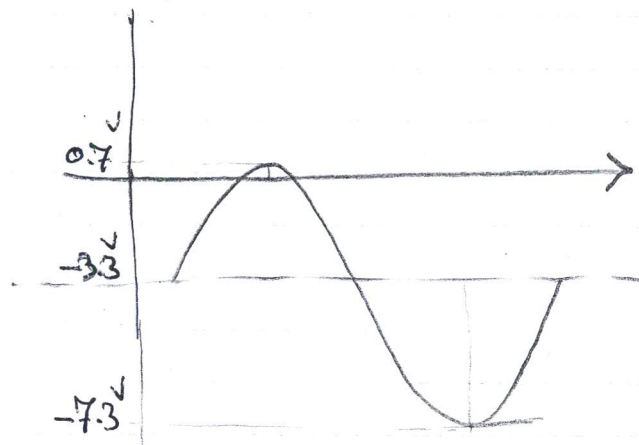
when D is R-B:  $V_{\text{out}} = V_{\text{in}} - V_c = V_{\text{in}} - V_p(\text{in}) + 0.7$

$$\therefore V_{\text{DC}} \approx -V_p(\text{in}) + 0.7 = -4 + 0.7 = -3.3\text{V}$$

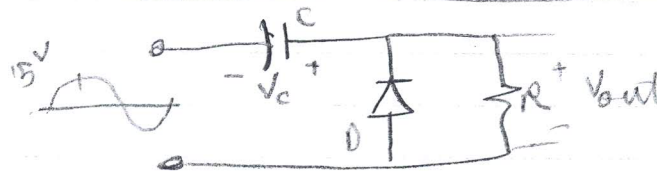
$$V_p^-(\text{out}) = V_p^-(\text{in}) - V_p(\text{in}) + 0.7 = -7.3\text{V}$$

$$V_p^+(\text{out}) = V_p^+(\text{in}) - V_p(\text{in}) + 0.7 = 0.7\text{V}$$

output is a sine-wave as follows:



b)

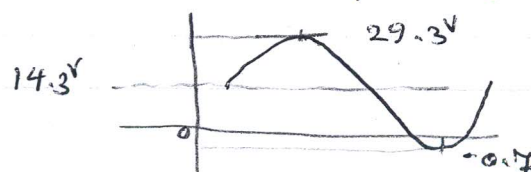


after charging:  $V_c = +V_p(\text{in}) - 0.7 =$

when D is R-B:  $V_{\text{out}} = V_{\text{in}} + V_c = V_{\text{in}} + V_p(\text{in}) - 0.7$

$$\therefore V_{\text{DC}} \approx V_p(\text{in}) - 0.7 = 14.3\text{V}$$

output is a sine-wave of the form:

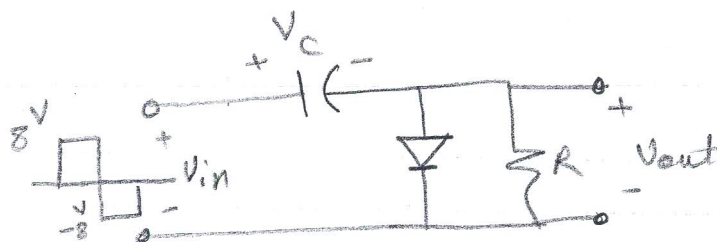


$$V_p^+(\text{out}) = 29.3\text{V}$$

$$V_p^-(\text{out}) = -0.7\text{V}$$



c)

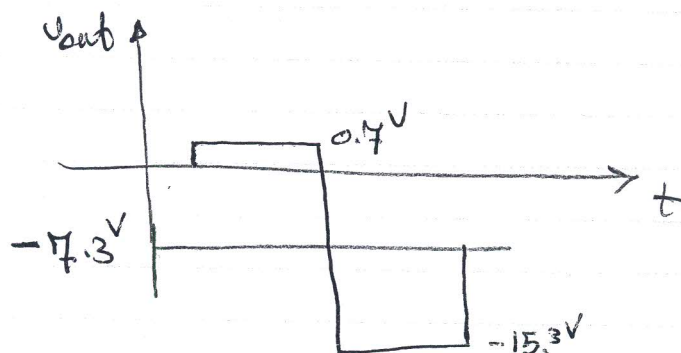


$$V_{DC} \cong -V_c = -(V_p(\text{in}) + 0.7) \\ = -8 + 0.7 = -7.3\text{V}$$

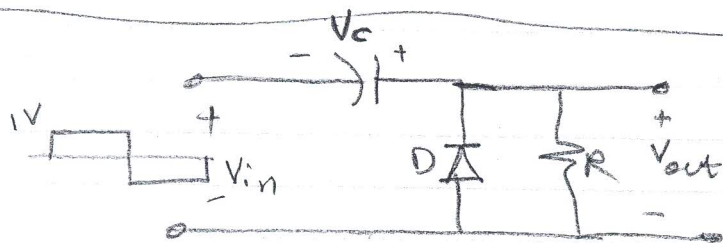
$$V_p^+(\text{out}) = V_p^+(\text{in}) - V_p(\text{in}) + 0.7 \\ = 8 - 8 + 0.7 = 0.7\text{V}$$

$$V_p^-(\text{out}) = V_p^-(\text{in}) - V_p(\text{in}) + 0.7 \\ = -8 - 8 + 0.7 = -15.3\text{V}$$

the output is a square wave of the form:



d)



$$V_{\text{out}} = V_c + V_{\text{in}} \\ \Rightarrow \text{+ve clamping}$$

$$V_{DC} \cong V_p(\text{in}) - 0.7 = 1 - 0.7 = 0.3\text{V}$$

$$V_p^+(\text{out}) = 1 + 0.3 = 1.3\text{V}$$

$$V_p^-(\text{out}) = -1 + 0.3 = -0.7\text{V}$$

The output is a square wave of the form :

