

# Ch. 9 HW solution

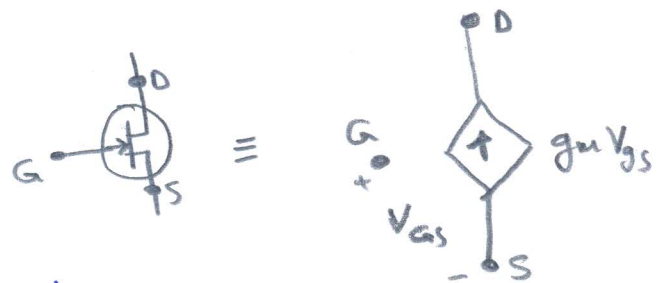
1

$$g_m = 6000 \mu S$$

$$\therefore I_D = g_m V_{GS}$$

$$a) I_D = 6000 \times 10^{-6} \times 10 \times 10^{-3} = 6 \times 10^{-5}$$

$$\therefore I_D = 60 \mu A$$



$$b) I_D = 6000 \mu S \times 150 \text{ mV} = 900 \mu A$$

$$c) I_D = 6000 \mu S \times 0.6 \text{ V} = 3.6 \text{ mA}$$

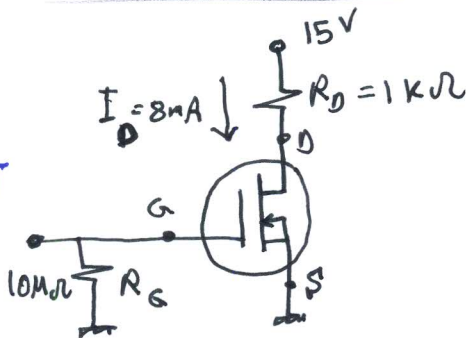
$$d) I_D = 6000 \mu S \times 1 \text{ V} = 6 \text{ mA}$$

5 & 6

a)

→ It is N-channel D-MOSFET  
→ Zero biased.

$$V_G = V_S = 0 \quad \therefore V_{GS} = 0$$

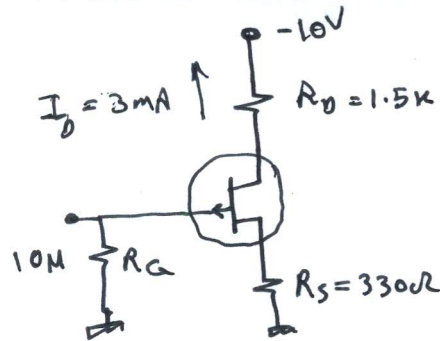


$$\therefore V_D = V_{DD} - I_D R_D = 15 - 8 \text{ mA} \times 1 \text{ k}$$

$$\therefore V_D = 7 \text{ V}$$

5 & 6

b)



→ It is P-channel FET  
→ self biased

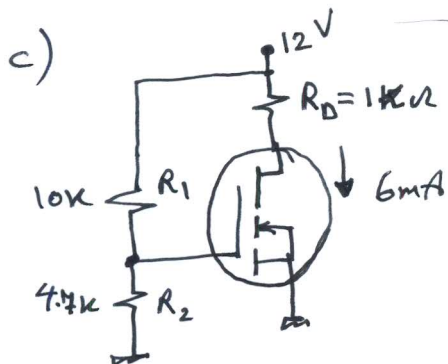
→  $V_G = 0$ ,  $V_S = -I_D R_D$   
 $= -3\text{mA} \times 1.5\text{k}\Omega$

$V_S = -4.5\text{V}$

$V_{GS} = 4.5\text{V}$

$V_D = -10 + 3\text{mA} \times 1.5\text{k}\Omega = -5.5$

$V_D = -5.5\text{V}$



→ It is N-channel E-MOSFET  
→ Voltage-divider bias

$V_G = \frac{R_2}{R_1 + R_2} V_{DD} = \frac{4.7}{14.7} \times 12$

$V_G = 3.837\text{V}$   
 $V_S = 0\text{V}$   
 $V_{GS} = 3.837\text{V}$   
 $V_D = 6\text{V}$

$V_D = 12 - 6 \times 10^{-3} \times 1 \times 10^3$

8

from the graph

at  $V_{GS} = -0.5$ :

$I_D \approx 3.9\text{mA}$

at  $V_{GS} = -3.5$ :

$I_D \approx 1.3\text{mA}$

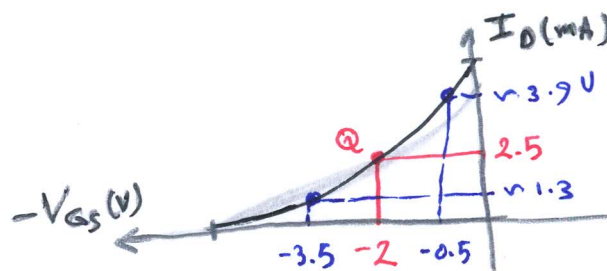


Fig. 9-16(a)

$I_{D(pp)} = 3.9 - 1.3 = 2.6\text{mA}$

[10]  $I_D = 2.83 \text{ mA}$ ,  $V_{GS(off)} = -4 \text{ V}$   
 $I_{DSS} = 8 \text{ mA}$

To get  $V_{GS}$ :

$$\therefore I_D = I_{DSS} \left( 1 - \frac{V_{GS}}{V_{GS(off)}} \right)^2$$

or (another soln)

$$V_S \approx I_D R_S = 2.83 \text{ mA} \times 1 \text{ k} = 2.83 \text{ V}$$

$$V_G = 0$$

$$\therefore V_{GS} = -2.83 \text{ V}$$

to get  $V_{DS}$ :

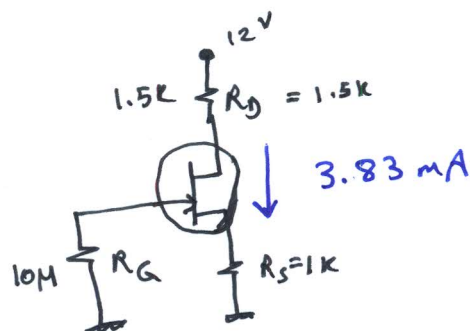
$$\therefore V_D = V_{DD} - I_D R_D = 12 - 2.83 \text{ mA} \times 1.5 \text{ k}$$

$$\therefore V_D = 7.755 \text{ V}$$

$$\therefore V_{DS} = 7.755 - 2.83$$

$$\therefore V_{DS} \approx 4.93 \text{ V}$$

DC-model of Fig. 9-56:



[12]  $g_m = 5000 \mu\text{S}$ ,  $V_{in} = 50 \text{ mV (rms)}$

$$\therefore A_v = \frac{V_{out}}{V_{in}} = g_m (R_D \parallel R_L)$$

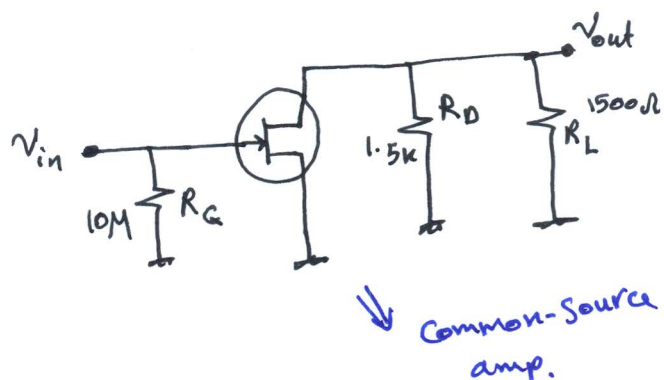
$$\therefore V_{out} = g_m (R_D \parallel R_L) V_{in}$$

$$= 5000 \mu\text{S} \times \frac{1500 \times 1500}{1500 + 1500} \times 50 \text{ mV}$$

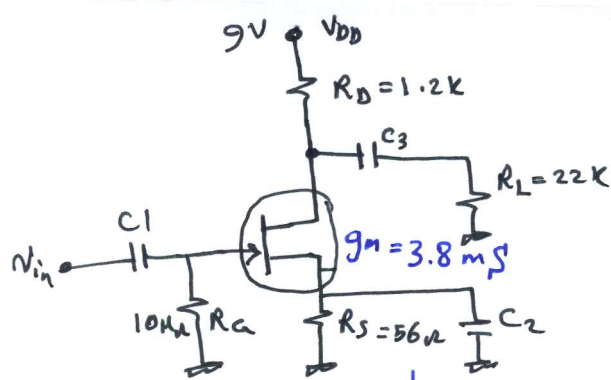
$$= 5000 \times 10^{-6} \times 450 \times 50 \times 10^{-3}$$

$$\therefore V_{out} = 187.5 \text{ mV rms}$$

AC-model of Fig. 9-56:



13 a)  $A_v = ??$

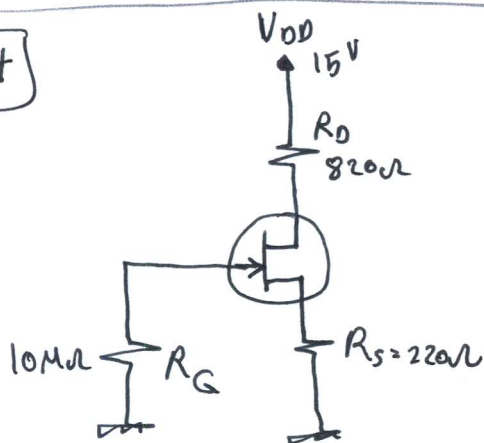


Common-source Amplifier

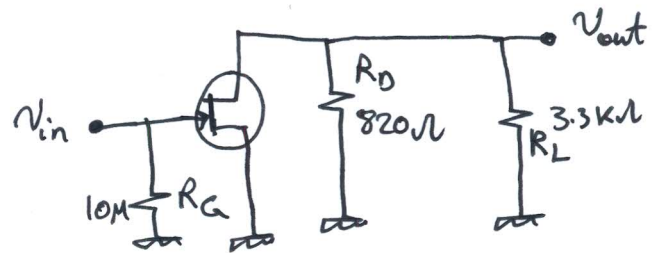
$$A_v = g_m (R_D \parallel R_L)$$

$$= 3.8 \times 10^{-3} \left( \frac{1.2 \times 22}{1.2 + 22} \right) \times 10^3 \quad \underline{\underline{4.32}}$$

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DC-equivalent cct.



AC equivalent cct.

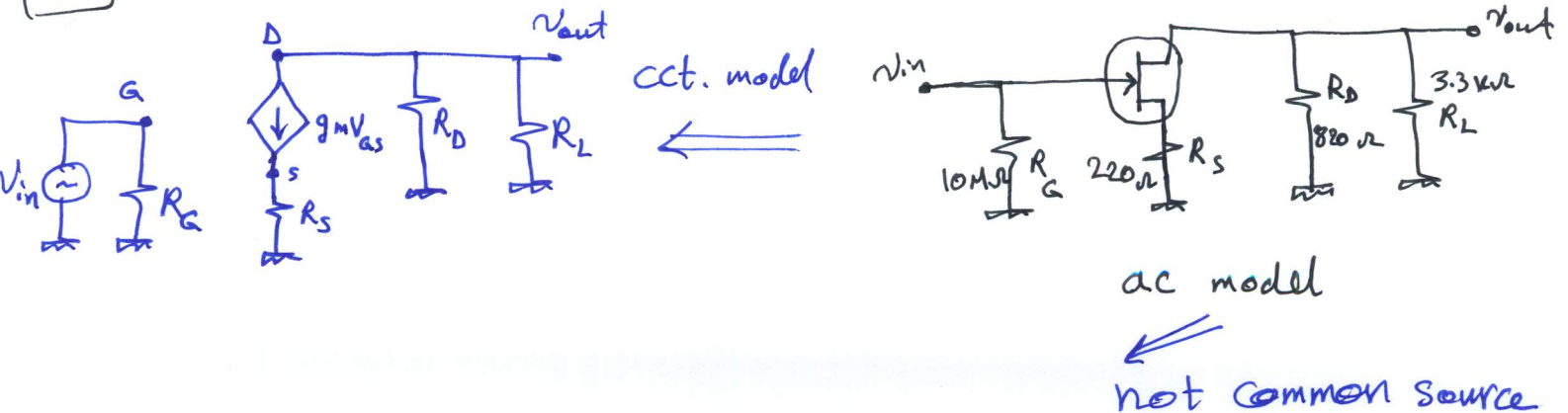
15

$$I_{DSS} = 15 \text{ mA}, V_{GS(off)} = -4, I_D = ??$$

Since, the Q-point is centered:

$$I_D = \frac{I_{DSS}}{2} = \underline{\underline{7.5 \text{ mA}}}$$

16



ac model

not common source



from eqv. cct model:

(5)

$$V_G = v_{in} \quad , \quad V_D = v_{out} = -g_m V_{GS} (R_D \parallel R_L) \quad , \quad V_S = g_m V_{GS} R_S$$

$$\therefore V_{GS} = V_G - V_S = v_{in} - g_m V_{GS} R_S$$

$$\text{or } v_{in} = (1 + g_m R_S) V_{GS}$$

$$\therefore A_V = \frac{v_{out}}{v_{in}} = \frac{-g_m V_{GS} (R_D \parallel R_L)}{1 + g_m R_S} \quad \therefore A_V = - \frac{g_m (R_D \parallel R_L)}{1 + g_m R_S}$$

→ To get  $g_m$ : assume dc-parameters of Q.15 (Q-point is centered)

$$\therefore I_D = 7.5 \text{ mA} \quad , \quad \therefore V_S = I_D R_S = 7.5 \text{ mA} \times 220 \Omega \quad , \quad V_G = 0$$

$$\therefore V_{GS} = -1.65 \text{ V}$$

$$\therefore g_m = \frac{2I_{DSS}}{|V_{GS(off)}|} \left( 1 - \frac{V_{GS}}{V_{GS(off)}} \right) = \frac{2 \times (15 \text{ m})}{4} \left( 1 - \frac{-1.65}{-4} \right)$$

$$\therefore g_m \approx 4.41 \text{ mS}$$

$$\therefore A_V = - \frac{4.41 \text{ mS} \times \frac{820 \times 3300}{820 + 3300}}{1 + 4.41 \text{ mS} \times 220} = -1.47$$

$$\text{or } |A_V| = 1.47$$

17  
assume the same  
gm of 16

$$A_V = g_m (R_D \parallel R_L \parallel 4.7 \text{ k}) = g_m \frac{1}{\frac{1}{R_D} + \frac{1}{R_L} + \frac{1}{4.7 \text{ k}}}$$

$$\therefore A_V = g_m \times (546.3) \\ = 4.41 \times 10^{-3} \times 546.3$$

$$\therefore A_V = 2.541$$

**18**  $I_{DSS} = 9 \text{ mA}$ ,  $V_{GS(off)} = -3 \text{ V}$   
centered Q-Point

dc equivalent ckt. :-

as centered Q-Point :

$$I_D = \frac{I_{DSS}}{2} = 4.5 \text{ mA}$$

$$V_G = 0 \text{ V}$$

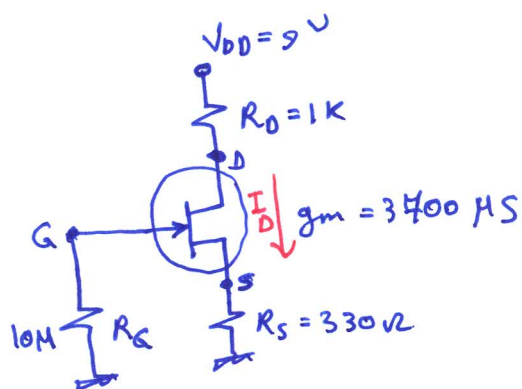
$$V_S = I_D R_S = 4.5 \times 10^{-3} \times 330 = 1.485 \text{ V}$$

$$V_{GS} = V_G - V_S = -1.485 \text{ V}$$

$$V_D = V_{DD} - I_D R_D = 9 - 4.5 \text{ mA} \times 1 \text{ k}\Omega = 4.5 \text{ V}$$

$$V_{DS} = 4.5 - (+1.485) = 3.015 \text{ V}$$

$$V_{GS} \approx -1.49 \text{ V}, V_{DS} \approx 3 \text{ V}$$



**22**  $g_m = 4.8 \text{ mS}$ ,  $I_{DSS} = 15 \text{ mA}$

① dc -analysis!

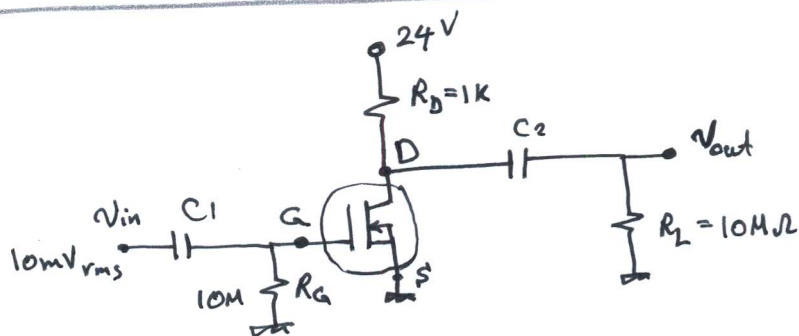
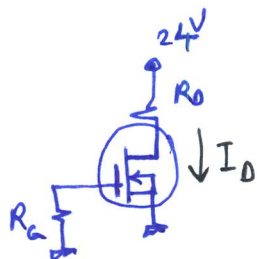
$$V_G = 0, V_S = 0$$

$$V_{GS} = 0$$

$$I_D = I_{DSS} = 15 \text{ mA}$$

$$V_D = V_{DD} - I_D R_D = 24 - 15 \text{ mA} \times 1 \text{ k}\Omega$$

$$V_{D1} = 9 \text{ V}_{dc}$$



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(7)

② ac - analysis:

$$\therefore A_v = g_m (R_D \parallel R_L)$$

$$\therefore A_v = 4.8 \times 10^{-3} * \left( \frac{10^3 * 10 * 10^6}{10^3 + 10 * 10^6} \right)$$

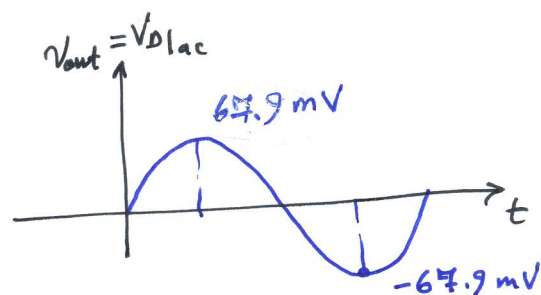
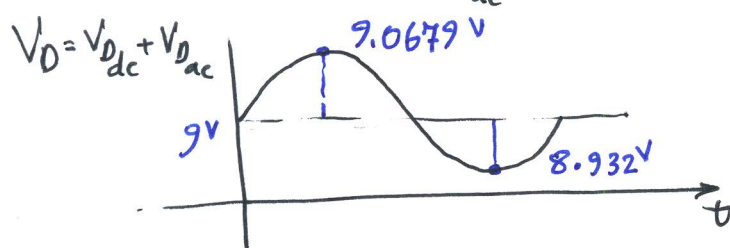
$$\therefore A_v \simeq 4.8$$

$$\therefore A_v = \frac{V_{out}}{V_{in}} \therefore V_{out} = A_v V_{in} = 4.8 * 10 \text{ mV}$$

$$\therefore V_{out} = 48 \text{ mV rms}$$

$$\therefore V_{out(p)} = \sqrt{2} * 48 \text{ mV} = 67.9 \text{ mV}$$

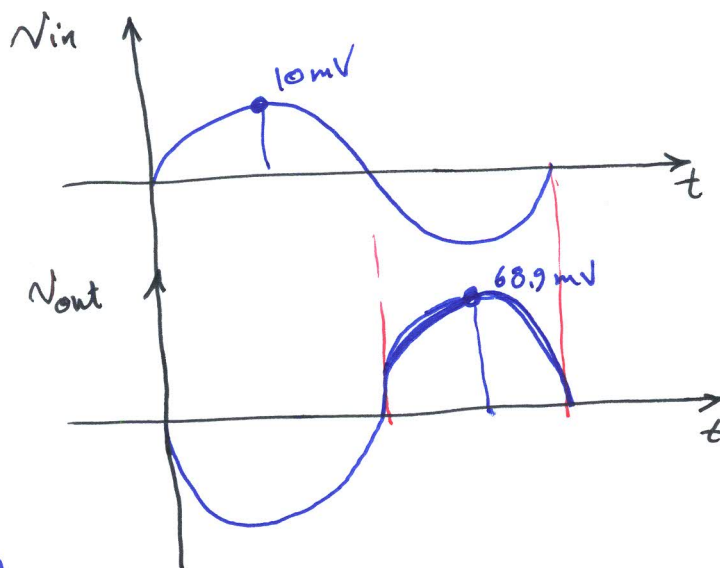
and  $V_{D1}(\text{Peak})_{ac} = 67.9 \text{ mV}$



⇒  
Don't forget  
that  $V_{out}$  is  
180° phase shift  
to  $V_{in}$

$$A_{v_i} = -g_m (R_D \parallel R_L)$$

exact



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$$I_{QSS} = 50 \mu A, V_{GS} = -15V$$

8

$$A_v = \frac{g_m (R_S \parallel R_L)}{1 + g_m (R_S \parallel R_L)}$$

$$\therefore R_S \parallel R_L = \frac{1.2k \times 1k}{1.2k + 1k} = 545.4 \Omega$$

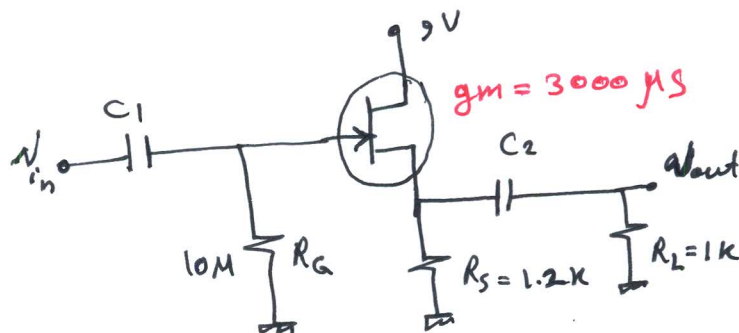
$$\therefore A_v = \frac{3000 \times 10^{-6} \times 545.4}{1 + 3000 \times 10^{-6} \times 545.4}$$

$$A_v \approx 0.621$$

$$\therefore R_{In} = R_G \parallel r_{gin} \quad ; \quad r_{gin} = \frac{|V_{GS}|}{I_{QSS}} = \frac{15}{50 \times 10^{-12}} = 3 \times 10^{11} \Omega$$

$$\therefore R_{In} = \frac{10 \times 10^6 \times 3 \times 10^{11}}{10^7 + 3 \times 10^{11}} = 9.99967 \times 10^6 \approx 10 M\Omega$$

$$R_{In} \approx 10 M\Omega$$



Common-drain amp.  
or  
Source follower

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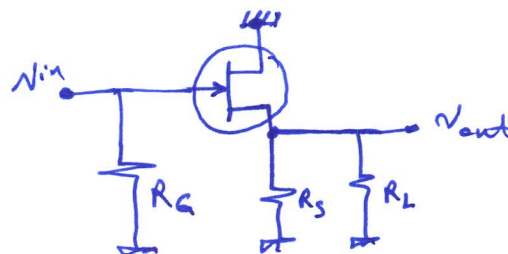
$$a) A_v = \frac{g_m (R_S \parallel R_L)}{1 + g_m (R_S \parallel R_L)}$$

$$R_S \parallel R_L = \frac{4.7 \times 4.7}{4.7 + 4.7} k\Omega = 4.243 k\Omega$$

$$\therefore A_v = \frac{3 \times 10^{-3} \times 4.243 \times 10^3}{1 + 3 mS \times 4.243 k\Omega}$$

$$A_v \approx 0.928$$

ac-equivalent ckt.:



$$b) R_S \parallel R_L = \frac{100 \times 1000}{100 + 1000} \Omega = 90.91 \Omega$$

$$A_v = \frac{4300 \times 10^{-6} \times 90.91}{1 + 4300 \times 10^{-6} \times 90.91}$$

$$A_v \approx 0.281$$



gate amp. /  $g_m = 4 \text{ mS}$  ,  $R_d = 1.5 \text{ k}\Omega$  ,  $A_v = ??$

(9)

$$\therefore A_v = g_m R_d$$

$$= 4 \text{ m} \times 1.5 \text{ k}$$

$$\therefore A_v = 6$$

[29]  $R_{in} = ??$

$$\therefore R_{in|source} = \frac{1}{g_m} = \frac{1}{4 \text{ mS}}$$

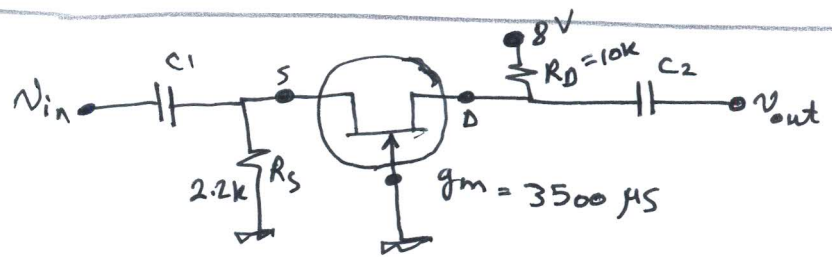
$$\therefore R_{in} = 250 \Omega$$

[30]  $A_v = ?$  ,  $R_{in} = ?$

$$A_v = g_m R_D$$

$$= 3500 \times 10^{-6} \times 10 \times 10^3$$

$$\therefore A_v = 35$$



↑ common gate amp.

$$R_{in} = R_S \parallel (R_{in|source}) ; R_{in|source} = \frac{1}{g_m} = 285.7 \Omega$$

$$\therefore R_{in} = \frac{2200 \times 285.7}{2200 + 285.7} = 252.86 \Omega$$

$$\therefore R_{in} \approx 253 \Omega$$