

LECTURE 11

THE FDTD METHOD – PART III

11. Yee's discrete algorithm

Maxwell's equations are discretized using central FDs. We set the magnetic loss equal to zero. Then,

$$\sigma_m = 0, \quad \mathbf{J}_m^i = 0$$

$$H_{x_i, j, k}^{n+0.5} = H_{x_i, j, k}^{n-0.5} - \frac{\Delta t}{\mu} \cdot \left[\frac{E_{z_i, j+1, k}^n - E_{z_i, j, k}^n}{\Delta y} - \frac{E_{y_i, j, k+1}^n - E_{y_i, j, k}^n}{\Delta z} \right]$$

$$H_{y_i, j, k}^{n+0.5} = H_{y_i, j, k}^{n-0.5} - \frac{\Delta t}{\mu} \cdot \left[\frac{E_{x_i, j, k+1}^n - E_{x_i, j, k}^n}{\Delta z} - \frac{E_{z_i+1, j, k}^n - E_{z_i, j, k}^n}{\Delta x} \right]$$

$$H_{z_i, j, k}^{n+0.5} = H_{z_i, j, k}^{n-0.5} - \frac{\Delta t}{\mu} \cdot \left[\frac{E_{y_i+1, j, k}^n - E_{y_i, j, k}^n}{\Delta x} - \frac{E_{x_i, j+1, k}^n - E_{x_i, j, k}^n}{\Delta y} \right]$$

11. Yee's discrete algorithm – cont.

$$E_{x_i, j, k}^{n+1} = k_E^E \cdot E_{x_i, j, k}^n + k_H^E \cdot \left[\frac{H_{z_i, j, k}^{n+0.5} - H_{z_i, j-1, k}^{n+0.5}}{\Delta y} - \frac{H_{y_i, j, k}^{n+0.5} - H_{y_i, j, k-1}^{n+0.5}}{\Delta z} - J_{eyi, j, k}^{i^{n+0.5}} \right]$$

$$E_{y_i, j, k}^{n+1} = k_E^E \cdot E_{y_i, j, k}^n + k_H^E \cdot \left[\frac{H_{x_i, j, k}^{n+0.5} - H_{x_i, j, k-1}^{n+0.5}}{\Delta z} - \frac{H_{z_i, j, k}^{n+0.5} - H_{z_i-1, j, k}^{n+0.5}}{\Delta x} - J_{eyi, j, k}^{i^{n+0.5}} \right]$$

$$E_{z_i, j, k}^{n+1} = k_E^E \cdot E_{z_i, j, k}^n + k_H^E \cdot \left[\frac{H_{y_i, j, k}^{n+0.5} - H_{y_i-1, j, k}^{n+0.5}}{\Delta x} - \frac{H_{x_i, j, k}^{n+0.5} - H_{x_i, j-1, k}^{n+0.5}}{\Delta y} - J_{ezi, j, k}^{i^{n+0.5}} \right]$$

$$k_E^E = \frac{1 - \frac{\sigma_e \Delta t}{2\epsilon}}{1 + \frac{\sigma_e \Delta t}{2\epsilon}} \quad k_H^E = \frac{\epsilon}{1 + \frac{\sigma_e \Delta t}{2\epsilon}} \quad \sigma_e \neq 0$$

11. Yee's discrete algorithm – cont.

The above coefficients are obtained by averaging the E -field, which appears in the loss term. For example,

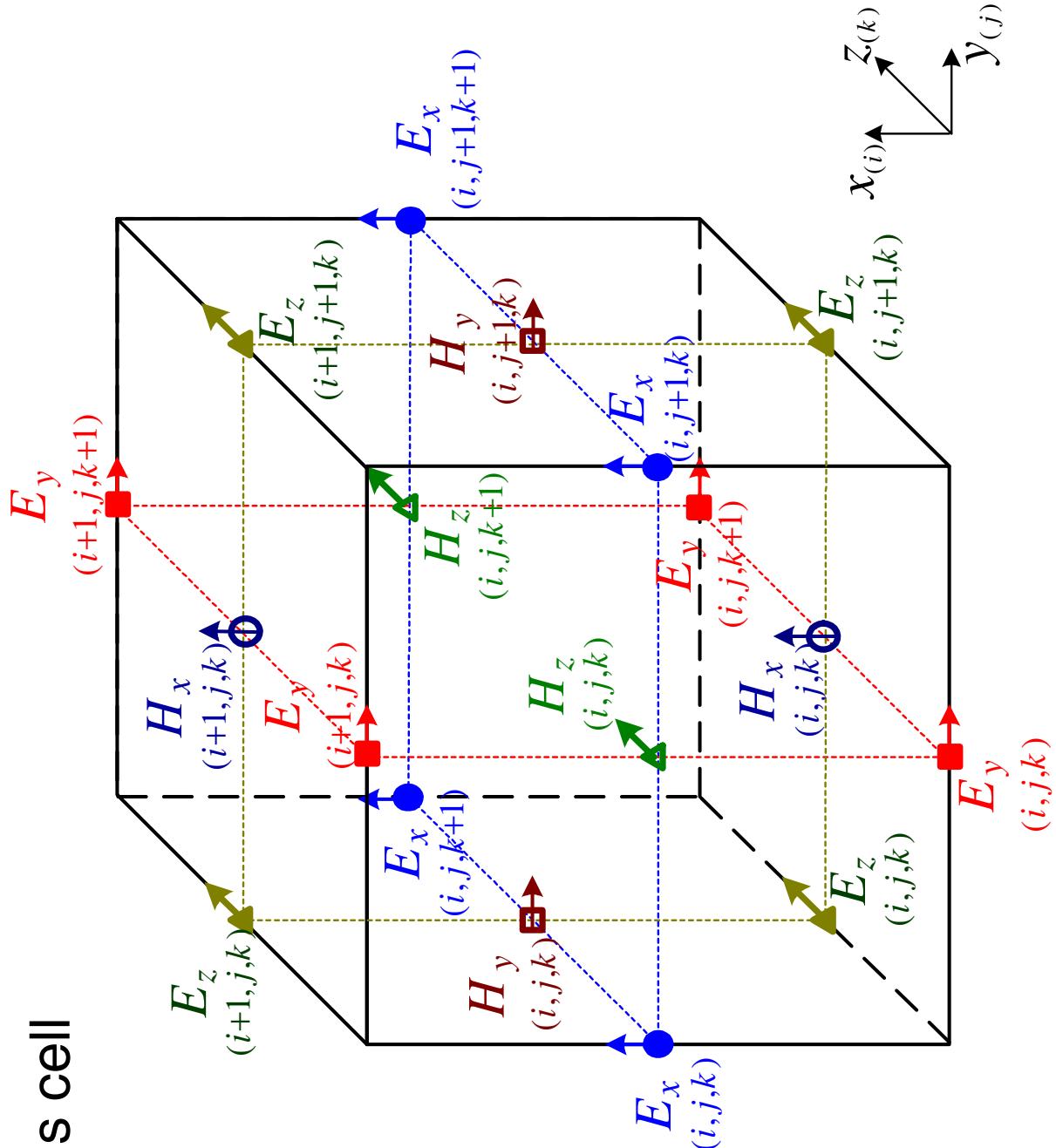
$$\epsilon \frac{\partial E_x}{\partial t} + \sigma_e E_x = \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} - J_{ex}^i \Rightarrow$$

$$\begin{aligned} \epsilon \frac{E_{x_i,j,k}^{n+1} - E_{x_i,j,k}^n}{\Delta t} + \sigma_e \frac{E_{x_i,j,k}^{n+1} + E_{x_i,j,k}^n}{2} &= \\ \frac{H_{z_i,j,k}^{n+0.5} - H_{z_i,j-1,k}^{n+0.5}}{\Delta y} - \frac{H_{y_i,j,k}^{n+0.5} - H_{y_i,j,k-1}^{n+0.5}}{\Delta z} - J_{ex,i,j,k}^i & \end{aligned}$$

The discretization steps in time and in space, as well as the numerical constant $\alpha = c \Delta t / \Delta h$ are determined as for the wave equation.

11. Yee's discrete algorithm – cont.

Yee's cell



11. Yee's discrete algorithm – cont.

2-D problems and their discretization

The 2-D TE_z mode

$$\mu \frac{\partial H_z}{\partial t} + \sigma_m H_z = - \left(\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} \right)$$

$$\epsilon \frac{\partial E_x}{\partial t} + \sigma_e E_x = \frac{\partial H_z}{\partial y} - J_{ex}^i$$

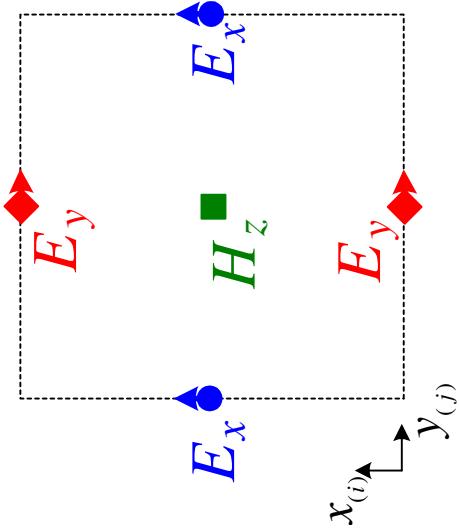
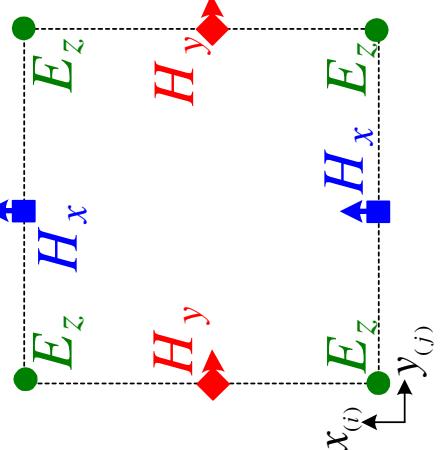
$$\epsilon \frac{\partial E_y}{\partial t} + \sigma_e E_y = - \frac{\partial H_z}{\partial x} - J_{ey}^i$$

The 2-D TM_z mode

$$\epsilon \frac{\partial E_z}{\partial t} + \sigma_e E_z = \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} - J_{ez}^i$$

$$\mu \frac{\partial H_x}{\partial t} + \sigma_m H_x = - \frac{\partial E_z}{\partial y}$$

$$\mu \frac{\partial H_y}{\partial t} + \sigma_m H_y = \frac{\partial E_z}{\partial x}$$



12. Absorbing (radiation) boundary conditions

ABCs constitute a special type of BCs, which simulate reflection-free propagation out of the computational domain. ABCs are necessary in open (radiation/scattering) problems, as well as in guided-wave problems where matched port terminations are needed.

The simplest to implement ABCs are associated with various approximations of a one-way plane wave propagation.

- One-way wave equation (Mur's ABC)
- Liao extrapolation
- Perfectly Matched Layers – basics
- Others: Higdon operator, Bayliss-Turkel annihilating operators, etc.

12. ABCs – cont.

A. The one-way wave equation (B. Engquist and A. Majda, “Absorbing boundary conditions for the numerical simulation of waves,” *Mathematics of Computation*, vol. 31, 1977, pp. 629-651)

This is an equation which permits wave propagation in only one direction. Consider the 3-D scalar wave equation

$$\frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2} - \frac{1}{c^2} \frac{\partial^2 f}{\partial t^2} = 0 \quad \Rightarrow \quad Lf = 0$$

The partial derivative operator is defined as

$$L = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} = \partial_x^2 + \partial_y^2 + \partial_z^2 - c^{-2} \partial_t^2$$

We wish to simulate propagation along $-x$ at $x=0$.

12. ABCs – cont.

The partial differential operator L can be factored, i.e., represented as sequentially applied two operators:

$$Lf = L^+ L^- f = 0$$

$$\begin{aligned}L^- &= \partial_x - c^{-1}\partial_t \sqrt{1-S^2} \\L^+ &= \partial_x + c^{-1}\partial_t \sqrt{1-S^2}\end{aligned}$$

The partial differential operators L^+ and L^- are pseudo-differential operators. They cannot be applied directly to a function. Formally, the equation

$$L^- f = 0$$

represents a wave traveling along $-x$, while the equation

$$L^+ f = 0$$

represents a wave traveling along $+x$.

12. ABCs – cont.

This becomes obvious in the case of a plane wave propagating along +/- X .

$$\partial_z = 0, \partial_y = 0 \Rightarrow S = 0 \quad \Rightarrow L^- = \partial_x - c^{-1}\partial_t, \quad L^+ = \partial_x + c^{-1}\partial_t$$

$$L^- f = \frac{\partial f}{\partial x} - \frac{1}{c} \frac{\partial f}{\partial t} = 0 \quad \text{Solution: } f(x + ct)$$

$$L^+ f = \frac{\partial f}{\partial x} + \frac{1}{c} \frac{\partial f}{\partial t} = 0 \quad \text{Solution: } f(x - ct)$$

The radical appearing in L^+ and L^- can be expanded using Taylor series

$$(1 - S^2)^{1/2} = 1 - \frac{1}{2}S^2 + O(S^4)$$

12. ABCs – cont.

If S^2 is very small, then $(1 - S^2)^{1/2} \approx 1$

The above is a **first-order approximation of S** . This means that the partial derivatives with respect to y and z are very small when compared with the partial derivative with respect to time scaled by the velocity of propagation c .

$$S^2 = \left(\frac{\partial_y}{c^{-1}\partial_t} \right)^2 + \left(\frac{\partial_z}{c^{-1}\partial_t} \right)^2$$

This happens when the wave is incident upon the $x=\text{const.}$ plane almost normally. The L -operator then becomes

$$\begin{aligned} L^{-1} &= \partial_x - c^{-1}\partial_t \\ \Rightarrow L^- f &= \partial_x f - c^{-1}\partial_t f = 0 \end{aligned}$$

12. ABCs – cont.

When the wave, however, impinges upon the $x=0$ boundary wall at larger angles, the 1st order approximation is very inaccurate. At grazing angles, S is large! For better accuracy, the **second-order approximation** can be used

$$(1 - S^2)^{1/2} \approx 1 - \frac{1}{2}S^2 \quad \longleftrightarrow \quad S^2 = \left(\frac{\partial_y}{c^{-1}\partial_t} \right)^2 + \left(\frac{\partial_z}{c^{-1}\partial_t} \right)^2$$

$$\begin{aligned} \text{The } L^- \text{- operator now becomes} \quad L^- &= \partial_x - c^{-1}\partial_t \left(1 - \frac{1}{2}S^2 \right) \\ \Rightarrow L^- &= \partial_x - c^{-1}\partial_t \left[1 - \frac{1}{2} \left(\frac{\partial_y}{c^{-1}\partial_t} \right)^2 - \frac{1}{2} \left(\frac{\partial_z}{c^{-1}\partial_t} \right)^2 \right] \end{aligned}$$

$$L^- = \partial_x - \frac{\partial_t}{c} + \frac{1}{2} \frac{c}{\partial_t} (\partial_{yy}^2 + \partial_{zz}^2)$$

Multiplying by ∂_t

12. ABCs – cont.

$$\begin{aligned}
 L^- f &= \partial_{xt}^2 f - \frac{1}{c} \partial_{tt}^2 f + \frac{c}{2} \left(\partial_{yy}^2 f + \partial_{zz}^2 f \right) = 0 & \text{at } x = 0 \\
 L^+ f &= \partial_{xt}^2 f + \frac{1}{c} \partial_{tt}^2 f - \frac{c}{2} \left(\partial_{yy}^2 f + \partial_{zz}^2 f \right) = 0 & \text{at } x = x_{\max} \\
 \\
 L^- f &= \partial_{yt}^2 f - \frac{1}{c} \partial_{tt}^2 f + \frac{c}{2} \left(\partial_{xx}^2 f + \partial_{zz}^2 f \right) = 0 & \text{at } y = 0 \\
 L^+ f &= \partial_{yt}^2 f + \frac{1}{c} \partial_{tt}^2 f - \frac{c}{2} \left(\partial_{xx}^2 f + \partial_{zz}^2 f \right) = 0 & \text{at } y = y_{\max} \\
 \end{aligned}$$

etc.

12. ABCs – cont.

Mur's ABC of 2nd Order (G. Mur, "Absorbing boundary conditions for the finite-difference approximation of the time-domain electromagnetic field equations," *IEEE Trans. Electromagnetic Compatibility*, vol. 23, 1981, pp. 377-382.

Mur implemented the above approximate expressions into finite-difference equations. Mur expands the partial derivatives in the L^+/L^- operators using central finite differences of the field component about an auxiliary grid point displaced half a step along the direction of absorption and along time.

Consider propagation along $-x$, at the $x=0$ boundary. We assume that the scalar function U is evaluated at integer spatial grid positions (i,j,k) and time positions n .

$$\partial_{xt}^2 f \Big|_{1/2,j,k}^n = \frac{1}{2\Delta t} \left(\frac{f_{1,j,k}^{n+1} - f_{0,j,k}^{n+1}}{\Delta x} - \frac{f_{1,j,k}^{n-1} - f_{0,j,k}^{n-1}}{\Delta x} \right)$$

12. ABCs – cont.

Now, the 2nd order time derivative has to be evaluated 1/2 step from the boundary as well. Mur averages the time derivatives at x=0 and x=1.

$$\partial_{tt}^2 f = \frac{1}{2} \left[\frac{f_{0,j,k}^{n+1} - 2f_{0,j,k}^n + f_{0,j,k}^{n-1}}{\Delta t^2} + \frac{f_{1,j,k}^{n+1} - 2f_{1,j,k}^n + f_{1,j,k}^{n-1}}{\Delta t^2} \right]$$

Now, the 2nd order y- and z- derivatives also have to be evaluated 1/2 step from the boundary. Mur averages those as well.

$$\begin{aligned} \partial_{yy}^2 f &= \frac{1}{2} \left[\frac{f_{0,j-1,k}^n - 2f_{0,j,k}^n + f_{0,j+1,k}^n}{\Delta y^2} + \frac{f_{1,j-1,k}^n - 2f_{1,j,k}^n + f_{1,j+1,k}^n}{\Delta y^2} \right] \\ \partial_{zz}^2 f &= \frac{1}{2} \left[\frac{f_{0,j,k-1}^n - 2f_{0,j,k}^n + f_{0,j,k+1}^n}{\Delta z^2} + \frac{f_{1,j,k-1}^n - 2f_{1,j,k}^n + f_{1,j,k+1}^n}{\Delta z^2} \right] \end{aligned}$$

12. ABCs – cont.

Substitute all the FD approximations above in

$$L^- f = \partial_{xt}^2 f - \frac{1}{c} \partial_{tt}^2 f + \frac{c}{2} \left(\partial_{yy}^2 f + \partial_{zz}^2 f \right) = 0$$

The result is

$$\begin{aligned} f_{0,j,k}^{n+1} &= -f_{0,j,k}^{n-1} + k_1 \left(f_{1,j,k}^{n+1} + f_{0,j,k}^{n-1} \right) + k_2 \left(f_{0,j,k}^n + f_{1,j,k}^n \right) + \\ &\quad + k_{3y} \left(f_{0,j-1,k}^n - 2f_{0,j,k}^n + f_{0,j+1,k}^n + f_{1,j-1,k}^n - 2f_{1,j,k}^n + f_{1,j+1,k}^n \right) + \\ &\quad + k_{3z} \left(f_{0,j,k-1}^n - 2f_{0,j,k}^n + f_{0,j,k+1}^n + f_{1,j,k-1}^n - 2f_{1,j,k}^n + f_{1,j,k+1}^n \right) \end{aligned}$$

$$k_1 = \frac{c_{\Delta t} - \Delta x}{c_{\Delta t} + \Delta x}$$

$$k_2 = \frac{(c_{\Delta t})^2 \Delta x}{2_{\Delta y}^2 (c_{\Delta t} + \Delta x)}$$

$$k_{3z} = \frac{(c_{\Delta t})^2 \Delta x}{2_{\Delta z}^2 (c_{\Delta t} + \Delta x)}$$

12. ABCs – cont.

Mur's ABC of 1st Order

To obtain Mur's approximation of

$$L^- f = \partial_x f - c^{-1} \partial_t f = 0$$

simply remove the 2nd order y - and z -derivatives from the formula above.

$$f_{0,j,k}^{n+1} = -f_{0,j,k}^{n-1} + k_1 \left(f_{1,j,k}^{n+1} + f_{0,j,k}^{n-1} \right) + k_2 \left(f_{0,j,k}^n + f_{1,j,k}^n \right)$$

$$k_1 = \frac{c \Delta t - \Delta x}{c \Delta t + \Delta x} \quad k_2 = \frac{2 \Delta x}{c \Delta t + \Delta x}$$

In Yee's algorithm, the E -field components tangential to the boundary are evaluated at this boundary. For example, at an $x=0$ boundary wall, the E_y and E_z field components define the boundary values of the EM field problem. Mur's ABC is applied to them.

12. ABCs – cont.

B. Liao's extrapolation (Z.P. Liao, H.L. Wong, B.P. Yang, and Y.F. Yuan, "A transmitting boundary for transient wave analyses," *Scientia Sinica (series A)*, vol. XXVII, 1984, pp. 1063-1076.)

The ABC known as Liao's ABC is easily explained as an extrapolation of the wave in space-time using Newton's backward-difference polynomial. It is an order less reflective than Mur's 2nd order ABC and does not depend strongly on the angle of incidence.

We now consider a boundary wall at x_{\max} . We assume that the field values are known for points located along a straight line perpendicular to the boundary. The objective is to find an approximation of the field at the boundary at the next time step $f(x_{\max}, t + \Delta t)$.

12. ABCs – cont.

The field values used for the approximation are obtained by a simultaneous shift in space-time:

$$\begin{aligned}m = 1 \quad f_1 &= f(x_{\max} - \delta c \Delta t, t) \\m = 2 \quad f_2 &= f(x_{\max} - 2\delta c \Delta t, t - \Delta t) \\m = 3 \quad f_3 &= f(x_{\max} - 3\delta c \Delta t, t - 2\Delta t) \\&\vdots\end{aligned}$$

$$m = N \quad f_N = f(x_{\max} - N\delta c \Delta t, t - (n-1)\Delta t)$$

Notice that such representation corresponds to a wave propagating in the +x direction: $f(x - ct)$

We aim at finding $f_0 = f(x_{\max}, t + \Delta t)$

12. ABCs – cont.

We now define backward finite-difference approximation
of p^{th} order at the point $\xi_1 = (x_{\max} - \alpha c_{\Delta t}, t)$.

$$\begin{aligned}
 D^1 f(\xi_1) &\equiv \Delta^1 f_1 = f_1 - f_2 \\
 D^2 f(\xi_1) &\equiv \Delta^2 f_1 = \Delta^1 f_1 - \Delta^1 f_2, & \Delta^1 f_2 &= f_2 - f_3 \\
 D^3 f(\xi_1) &\equiv \Delta^3 f_1 = \Delta^2 f_1 - \Delta^2 f_2, & \Delta^2 f_2 &= \Delta^1 f_2 - \Delta^1 f_3 \\
 &\vdots & \Delta^1 f_3 &= f_3 - f_4 \\
 D^N f(\xi_1) &\equiv \Delta^N f_1 = \Delta^{N-1} f_1 - \Delta^{N-1} f_2
 \end{aligned}$$

$$f_m = f(\xi_m) = f(x_{\max} - m \delta c_{\Delta t}, t - (m-1) \Delta t)$$

12. ABCs – cont.

The N -th backward difference can be written in terms of the function values as

$$\Delta^N f_1 = \sum_{m=1}^{N+1} (-1)^{m-1} C_{m-1}^N f_m,$$

where the Newton binomial coefficients are

$$C_{m-1}^N = \binom{N}{m-1} = \frac{N!}{(N-m+1)!(m-1)!}$$

Alternatively, a function can be expressed (interpolated) in terms of the backward finite differences at f_1

$$\begin{aligned} f_m &\equiv f_1 + \frac{\beta(\beta+1)}{2!} \Delta^2 f_1 + \frac{\beta(\beta+1)(\beta+2)}{3!} \Delta^3 f_1 + \dots \\ &+ \frac{\beta(\beta+1)\cdots(\beta+N-2)}{(N-1)!} \Delta^{N-1} f_1, \quad 1 \leq m \leq N, \quad \beta = 1 - m \end{aligned}$$

12. ABCs – cont.

We now use the above formula to extrapolate the function values, and we set $m = 0$. Then, $\beta = 1$.

$$f_0 = f(t + \Delta t, x_{\max}) \equiv f_1 + \Delta^1 f_1 + \Delta^2 f_1 + \Delta^3 f_1 + \cdots + \Delta^{N-1} f_1$$

This is Liao's ABC. Liao *et al.* showed that for a sinusoidal plane wave of unit amplitude and wavelength λ , the maximum error is given by

$$|\Delta^N f|_{\max} = 2^N \sin^N(\pi c \Delta t / \lambda)$$

Assuming that

$$\Delta h = 2c \Delta t \quad \text{and} \quad \Delta h = \lambda / 32$$

the error is estimated at 0.1%. Liao's ABC is robust and depends little on the angle if incidence. With orders higher than $N=3$, however, it sometimes causes instabilities.

12. ABCS – cont.

$$f_0 = f(t + \Delta t, x_{\max}) \equiv f_1 + \Delta^1 f_1 + \Delta^2 f_1 + \Delta^3 f_1 + \cdots + \Delta^{N-1} f_1$$

Liao's ABC is simple to implement.

```

! ABC in MAIN
ix2=nt-((nt-1)/2)*2
ix3=nt-((nt-1)/3)*3
ix4=nt-((nt-1)/4)*4
                                ! before end of cycle
                                ! history
                                A2_B(:,:,ix2)=AX(:,:,3)
                                A3_B(:,:,ix3)=AX(:,:,4)
                                A4_B(:,:,ix4)=AX(:,:,5)
*****                                *****

F0=>AX(:,:,nk);F1=>AX(:,:,nk-1)    ! front, ABC
F2=>A2_F(:,:,ix2);F3=>A3_F(:,:,ix3);F4=>A4_F(:,:,ix4)
call LIAO(ni,nj)
*****                                *****

subroutine LIAO(dim1,dim2)

D1=F1-F2;D2=F2-F3;D3=F3-F4
DD1=D1-D2;DD2=D2-D3
DDD1=DD1-DD2
                                ! define variables
                                real(8),dimension(ni,nj,2),target:: A2_F,A2_B
                                real(8),dimension(ni,nj,3),target:: A3_F,A3_B
                                real(8),dimension(ni,nj,4),target:: A4_F,A4_B
                                real(8),dimension(:,:,),pointer:: F0,F1,F2,F3,F4
*****                                *****

```

```

D1=F1-F2;D2=F2-F3;D3=F3-F4
DD1=D1-D2;DD2=D2-D3
DDD1=DD1-DD2
                                ! define variables
                                real(8),dimension(ni,nj,2),target:: A2_F,A2_B
                                real(8),dimension(ni,nj,3),target:: A3_F,A3_B
                                real(8),dimension(ni,nj,4),target:: A4_F,A4_B
                                real(8),dimension(:,:,),pointer:: F0,F1,F2,F3,F4
*****                                *****
F0=F1+DD1+DDD1
return
end subroutine LIAO

```

Important topics not discussed in this overview lecture

- Perfectly Matched Layer ABC
- FDTD on curvilinear grids
- FDTD in dispersive and anisotropic media
- FDTD in nonlinear and gain materials
- Integrating lumped elements with the FDTD full-wave analysis
- Near-to-Far-Field transformation for antenna radiation patterns
- Modified implicit FDTD schemes – the FDTD-ADI