

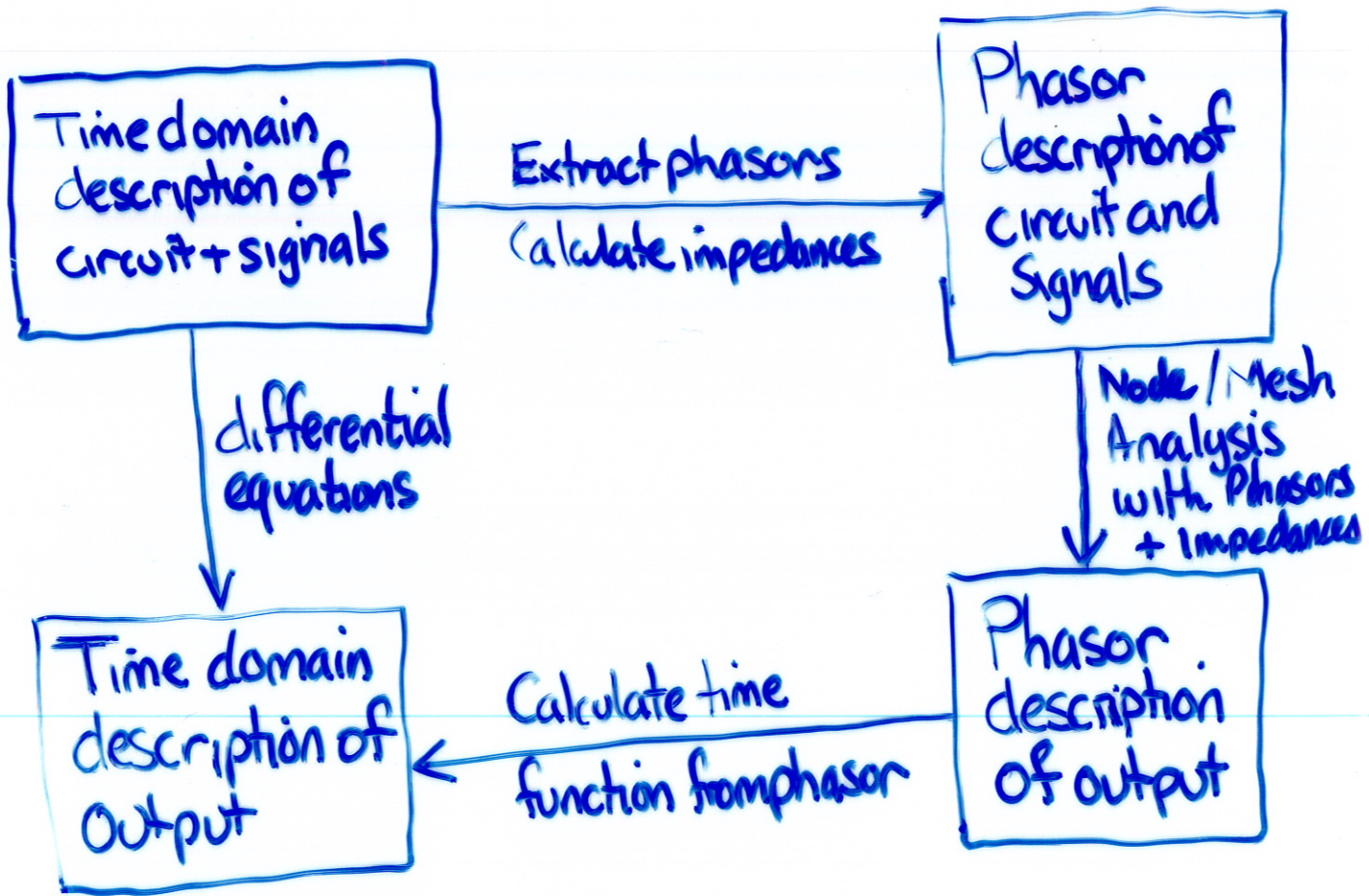
## IMPACT OF PHASOR RELATIONSHIPS.

Recall

$$\begin{aligned} A \cos(\omega t + \theta) &= \operatorname{Re}\{A e^{j(\omega t + \theta)}\} \\ &= \operatorname{Re}\{A e^{j\theta} e^{j\omega t}\} \end{aligned}$$

$A e^{j\theta}$  is the phasor representation of  
 $A \cos(\omega t + \theta)$

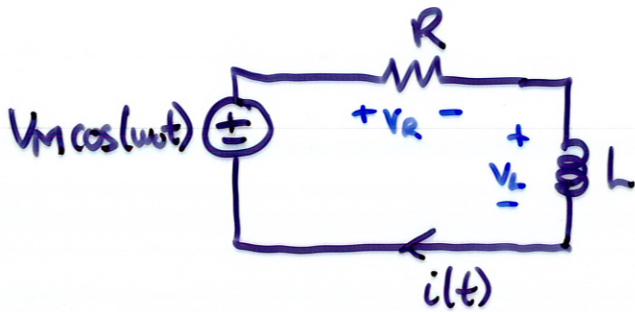
# Simplified Analysis of Linear Circuits with Sinusoidal inputs in steady-state using phasors



Why does this work?

How do phasors allow us to avoid differential equations?

FIND THE FORCED RESPONSE:



$$\text{KVL} \quad -V_m \cos(\omega t) + v_R(t) + v_L(t) = 0$$

$$\Rightarrow v_L(t) + v_R(t) = V_m \cos(\omega t)$$

$$\Rightarrow L \frac{di(t)}{dt} + R i(t) = V_m \cos(\omega t)$$

Postulate form of forced response

$$i(t) = A_1 \cos(\omega t) + A_2 \sin(\omega t)$$

Substitute into differential equation

$$\begin{aligned} -A_1 L \omega \sin(\omega t) + A_2 L \omega \cos(\omega t) + R A_1 \cos(\omega t) + R A_2 \sin(\omega t) \\ = V_m \cos(\omega t) \end{aligned}$$

Equating coeffs of sin and cosine

$$-A_1 L \omega + R A_2 = 0$$

$$A_2 L \omega + R A_1 = V_m$$

Solution:

$$A_1 = \frac{R V_M}{R^2 + \omega_0^2 L^2} \quad ; \quad A_2 = \frac{\omega_0 L V_M}{R^2 + \omega_0^2 L^2}$$

⇒

$$i(t) = \frac{R V_M}{R^2 + \omega_0^2 L^2} \cos(\omega_0 t) + \frac{\omega_0 L V_M}{R^2 + \omega_0^2 L^2} \sin(\omega_0 t)$$

$$= \frac{V_M}{\sqrt{R^2 + \omega_0^2 L^2}} \cos\left(\omega_0 t - \arctan\left(\frac{\omega_0 L}{R}\right)\right)$$

⇒ Forced response is also a sinusoid ~~with~~ with same frequency, but

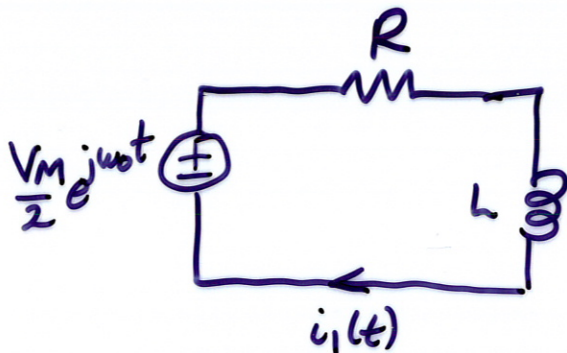
- ① Different amplitude
- ② Different phase

Phasors capture amplitude and phase.

Can we use them to make this easier?

$$V_m \cos(\omega t) = \frac{V_m}{2} e^{j\omega t} + \frac{V_m}{2} e^{-j\omega t}$$

Let's try a super position approach



$$L \frac{di_1(t)}{dt} + Ri_1(t) = \frac{V_m}{2} e^{j\omega t}$$

Postulate form of forced response

$$i_1(t) = I_m e^{j(\omega t + \phi)}$$

Substitute into differential equation

$$j\omega L I_m e^{j(\omega t + \phi)} + R I_m e^{j(\omega t + \phi)} = \frac{V_m}{2} e^{j\omega t}$$

Divide by  $e^{j\omega t}$

$$j\omega L I_m e^{j\phi} + R I_m e^{j\phi} = \frac{V_m}{2}$$

$$\begin{aligned}
 \Rightarrow I_m e^{j\phi} &= \frac{V_m/2}{R + j\omega_0 L} \\
 &= \frac{V_m/2}{\sqrt{R^2 + \omega_0^2 L^2}} e^{j \tan^{-1}(\omega_0 L/R)} \\
 &= \frac{V_m/2}{\sqrt{R^2 + \omega_0^2 L^2}} e^{-j \tan^{-1}(\omega_0 L/R)}
 \end{aligned}$$

$$\Rightarrow i_1(t) = \frac{V_m/2}{\sqrt{R^2 + \omega_0^2 L^2}} e^{j(\omega_0 t - \tan^{-1}(\omega_0 L/R))}$$

Similarly

$$i_2(t) = \frac{V_m/2}{\sqrt{R^2 + \omega_0^2 L^2}} e^{-j(\omega_0 t - \tan^{-1}(\omega_0 L/R))}$$

$$\Rightarrow i(t) = \frac{V_m}{\sqrt{R^2 + \omega_0^2 L^2}} \cos(\omega_0 t - \tan^{-1}(\omega_0 L/R))$$

Now let's try by phasor analysis

$$L \frac{di(t)}{dt} + Ri(t) = V_m \cos(\omega t)$$

$$V_m \cos(\omega t) = \operatorname{Re} \{ V e^{j\omega t} \} \quad V = V_m$$

Postulate  $i(t) = \operatorname{Re} \{ I e^{j\omega t} \} \quad I = I_m e^{j\phi}$

- Approach
- ① Solve differential equation in complex case
  - ② Take the real part at the end.

Substitute  $I e^{j\omega t}$  into differential equation

$$j\omega L I e^{j\omega t} + R I e^{j\omega t} = V e^{j\omega t}$$

Divide by  $e^{j\omega t}$

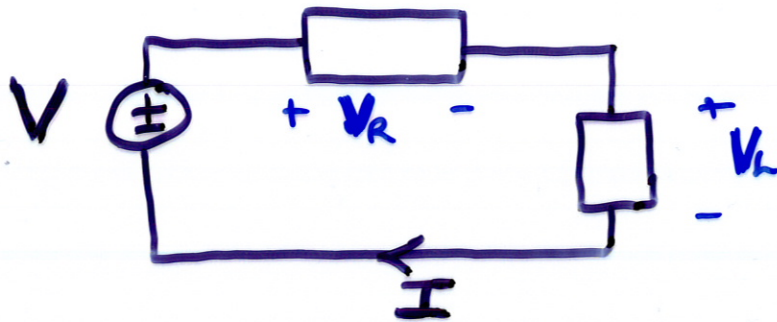
$$j\omega L I + R I = V$$

Differential eqn  
has become  
algebraic!

$$\Rightarrow I = \frac{V_m}{R + j\omega L} = \frac{V_m}{\sqrt{R^2 + \omega^2 L^2}} e^{-j \operatorname{atan}(\omega L/R)}$$

$$\Rightarrow i(t) = \frac{V_m}{\sqrt{R^2 + \omega^2 L^2}} \cos(\omega t - \operatorname{atan}(\omega L/R))$$

Can we use phasors directly?



$$\text{KVL} \quad -V + V_R + V_L = 0$$

$$V = V_m e^{j\omega t}$$

$$V_R = R \mathbf{I}$$

$$V_L = j\omega L \mathbf{I}$$

$$\Rightarrow (R + j\omega L) \mathbf{I} = V_m$$

$$\Rightarrow \mathbf{I} = \frac{V_m}{R + j\omega L} = \frac{V_m}{\sqrt{R^2 + \omega^2 L^2}} e^{-j \tan^{-1}(\omega L/R)}$$

$$\Rightarrow i(t) = \frac{V_m}{\sqrt{R^2 + \omega^2 L^2}} \cos(\omega t - \tan^{-1}(\omega L/R))$$