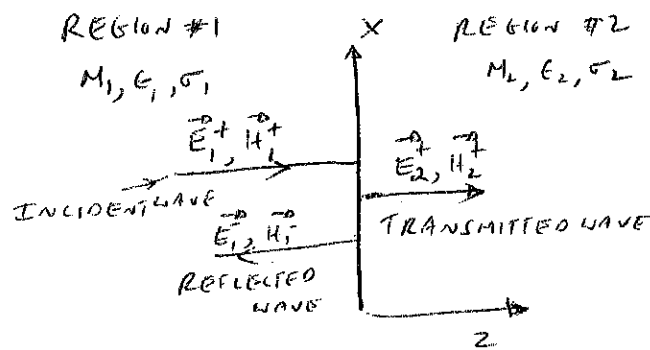


# PLANE WAVE REFLECTION



CONSIDER THE INTERFACE BETWEEN TWO REGIONS. HERE, THE REGIONS COULD BE ANY TYPE OF MEDIUMS - DIELECTRIC OR CONDUCTORS.

SUPPOSE THAT ~~ENERGY~~ <sup>A</sup> WAVE IS INCIDENT AT THE BOUNDARY FROM LEFT ( $z < 0$ ). ~~THE~~ ~~ELECTRIC~~ & MAGNETIC FIELDS OF THE INCIDENT WAVE ARE

$$\vec{E}_1^+ = E_{x1}^+ \hat{x} ; \quad \vec{H}_1^+ = H_{y1}^+ \hat{y}$$

HERE, THE SUPERSCRIPT '+' INDICATES IT IS TRAVELLING IN THE +ve z-DIRECTION & THE SUBSCRIPT '1' ~~INDICATES~~ CORRESPONDS TO THE REGION #1. LET

$$E_{x1}^+ = \text{Re} \{ E_{xs1}^+ e^{j\omega t} \}$$

$$H_{y1}^+ = \text{Re} \{ H_{ys1}^+ e^{j\omega t} \}$$

$$E_{xs1}^+ = A_1^+ e^{-j\beta_1 z}$$

$$E_{xs1}^+ = A_1^+ e^{-\alpha_1 z} \cos(\omega t - \beta_1 z)$$

①  
REFER TO  
PREVIOUS  
NOTES.

$$H_{yS1}^+(z) = \frac{A_1^+}{n_1} e^{-jk_1 z} \quad \text{--- (2)}$$

$$H_{y1}^+ = \frac{A_1^+}{n_1} e^{-\alpha_1 z} \cos(\omega t - \beta_1 z)$$

HERE, WE TAKE  $A_1^+$  AS REAL.  $k_1$  &  $n_1$  ARE COMPLEX IN GENERAL. THE WAVE IS TRANSMITTED TO REGION 2 AND ELECTRIC & MAGNETIC FIELDS IN REGION 2 ARE

$$E_{xS2}^+(z) = A_2^+ e^{-jk_2 z} \quad \text{--- (3)}$$

$$H_{yS2}^+(z) = \frac{A_2^+}{n_2} e^{-jk_2 z}$$

LET US SUPPOSE THE ENERGY OF THE INCIDENT WAVE IS TRANSMITTED TO REGION 2 WITHOUT REFLECTION AT THE BOUNDARY. WE MUST SATISFY THE BOUNDARY CONDITIONS AT  $z=0$ .

TANGENTIAL COMPONENTS OF  $\vec{E}$  SHOULD BE CONTINUOUS AT THE BOUNDARY. SINCE  $\vec{E}$  IS POLARIZED ALONG  $\vec{x}$ , THE FIELD IS TANGENT TO THE SURFACE. AT  $z=0$ , FROM (1) & (3), WE HAVE

$$E_{xS1}^+ = E_{xS2}^+ \Rightarrow A_1^+ = A_2^+ \quad \text{--- (4)}$$

SIMILARLY, TANGENTIAL COMPONENTS OF  $\vec{H}$  SHOULD BE CONTINUOUS.

$\vec{H}$ , BEING  $y$ -DIRECTED, IS ALSO TANGENT TO THE BOUNDARY SURFACE. AT  $z=0$ ,

$$H_{yS1}^+ = H_{yS2}^+ \Rightarrow \frac{A_1^+}{n_1} = \frac{A_2^+}{n_2} \Rightarrow n_1 = n_2 \Rightarrow \text{--- (5)}$$

(3)

THIS MEANS THAT THE MATERIALS ON BOTH SIDES OF THE BOUNDARY SHOULD BE THE SAME (i.e. NO BOUNDARY)

TO HAVE NO REFLECTION. IN OTHER WORDS, WE ARE NOT ABLE TO SATISFY THE BOUNDARY CONDITIONS WHEN TWO DIFFERENT MATERIALS ( $\eta_1 \neq \eta_2$ ) ARE PRESENT, & ~~NO~~ <sup>IN THE</sup> ~~REFLECTION~~ ABSENCE OF REFLECTION.

NEXT, LET US CONSIDER THE CASE IN WHICH THE INCIDENT WAVE IS PARTIALLY TRANSMITTED & THE REST IS REFLECTED. THE REFLECTED FIELD IS

$$E_{x1}^- = A_1^- e^{j k_1 z} \rightarrow \text{⑥} \quad \text{BACKWARD PROPAGATING WAVE}$$

$$H_{y1}^- = -\frac{A_1^-}{\eta_1} e^{j k_1 z} \rightarrow \text{⑦} \quad \begin{array}{l} \text{Poynting vector} \\ \vec{E}^- \times \vec{H}^- \text{ SHOULD BE} \\ \text{IN } -\hat{z} \text{ DIRECTION} \end{array}$$

SO, <sup>THE</sup> TOTAL FIELD IN REGION 1 IS

$$E_{x1} = E_{x1}^+ + E_{x1}^-$$

$$= A_1^+ e^{-j k_1 z} + A_1^- e^{j k_1 z} \rightarrow \text{⑧}$$

$$H_{y1} = H_{y1}^+ + H_{y1}^-$$

$$= \frac{A_1^+}{\eta_1} e^{-j k_1 z} - \frac{A_1^-}{\eta_1} e^{j k_1 z} \rightarrow \text{⑨}$$

(4)

CONTINUITY OF THE TANGENTIAL COMPONENT OF  $\vec{E}$  &  $\vec{H}$   
 AT THE BOUNDARY ( $z=0$ ) IMPLIES, ((<sup>IN</sup> EQS. (3), (4), (6) & (7), SET  $z=0$ ))

$$A_1^+ + A_1^- = A_2^+ \rightarrow (8)$$

$$\frac{A_1^+ - A_1^-}{\eta_1} = \frac{A_2^+}{\eta_2} \rightarrow (9)$$

$$(8) + \eta_1 \times (9) \Rightarrow 2A_1^+ = A_2^+ \left(1 + \frac{\eta_1}{\eta_2}\right) = A_2^+ \frac{\eta_1 + \eta_2}{\eta_2}$$

~~THE RATIO OF~~  $\rightarrow (10)$

THE RATIO OF THE AMPLITUDES OF THE TRANSMITTED & INCIDENT  
 FIELDS DEFINES THE TRANSMISSION COEFFICIENT,  $\tau$

$$\tau = \frac{A_2^+}{A_1^+} = \frac{2\eta_2}{\eta_1 + \eta_2} = |\tau| e^{j\phi_\tau} \rightarrow (11)$$

ELIMINATING  $A_2^+$  IN EQ. (8) BY USING EQ. (11), WE GET

$$A_1^+ + A_1^- = \frac{2\eta_2}{\eta_1 + \eta_2} A_1^+$$

$$A_1^- = \left(\frac{2\eta_2}{\eta_1 + \eta_2} - 1\right) A_1^+ = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} A_1^+$$

(5)

THE RATIO OF THE AMPLITUDE OF REFLECTED FIELD TO

INCIDENT FIELD IS DEFINED AS REFLECTION COEFFICIENT,

$\Gamma$ ,

$$\Gamma = \frac{A_1^-}{A_1^+} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} = |\Gamma| e^{j\phi_\Gamma} \rightarrow (12)$$

DIVIDING EQ. (8) BY  $A_1^+$ , WE HAVE

$$1 + \frac{A_1^-}{A_1^+} = \frac{A_2^+}{A_1^+} \Rightarrow \boxed{1 + \Gamma = \tau} \rightarrow (13)$$

SPECIAL CASES:

REGION 1 : PERFECT DIELECTRIC

REGION 2 : PERFECT CONDUCTOR

FOR A PERFECT CONDUCTOR,  $\sigma = \infty$ ;

$$\therefore \eta_2 = \sqrt{\frac{j\omega\mu_2}{\sigma_2 + j\omega\epsilon_2}} \rightarrow 0 \text{ SINCE } \sigma_2 = \infty.$$

NOW, EQ. (12) AND (13) BECOME

$$\Gamma = -1 \rightarrow (14)$$

$$\tau = 0 \rightarrow (15)$$

FROM EQ. (11),  $\tau = 0 \Rightarrow A_2^+ = 0 \Rightarrow$  EM WAVE IS NOT TRANSMITTED TO THE PERFECT CONDUCTOR & THE INCIDENT WAVE IS FULLY REFLECTED. ANOTHER WAY TO LOOK AT THIS

(6)

IS TO NOTE THAT THE SKIN DEPTH IS ZERO

$$\Gamma = -1 \Rightarrow A_1^- = -A_1^+ \rightarrow (16)$$

$|A_1^-| = |A_1^+| \Rightarrow$  THE AMPLITUDES OF

INCIDENT & REFLECTED FIELDS ARE EQUAL. -VE SIGN IN

EQ. (16) INDICATES THAT AT THE BOUNDARY, THE REFLECTED

FIELD IS SHIFTED IN PHASE BY  $180^\circ$  RELATIVE TO THE

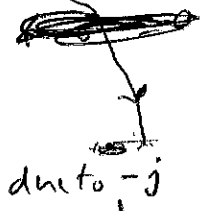
INCIDENT FIELD. TOTAL FIELD IN REGION 1 IS

$$\begin{aligned} E_{x1} &= E_{x1}^+ + E_{x1}^- \\ &= A_1^+ \left( \frac{e^{-jk_1 z} - e^{jk_1 z}}{2j} \right) 2j \end{aligned}$$

$$= -2j A_1^+ \sin(k_1 z)$$

FOR A PERFECT (LOSSLESS) DIELECTRIC,  $\epsilon$  IS REAL

$$k_1 = \omega \sqrt{\mu_0 \epsilon_0} \text{ IS REAL.}$$



$$E_{x1} = \text{Re} \left\{ E_{x1} e^{j\omega t} \right\} = 2 \text{Re} \left\{ A_1^+ e^{j(\omega t + j\pi/2)} \right\} \times \sin(k_1 z)$$

$$E_{x1} = 2A_1^+ \sin k_1 z \sin \omega t$$